





# Introduction of the «Ropes» Group **OITAF-Recommendation "Rope Lifetime" Historical Introduction**

Dr.-Ing. Konstantin Kuehner konstantin.kuehner@jakob.eu



## Introduction of Work Committee (WC) II «Ropes»



Chairman: Sven Winter Vice Chair / Protocol: Stéphane Pernot

#Manufacturers: Doppelmayr, Leitner Ropeways, Fatzer, Jakob Rope Systems, Teufelberger-Redaelli, Usha Martin

#Testing Bodies: IFT University of Stuttgart, IWM,

Letscan, ROTEC, TÜV SÜD, TVFA

#Authorities: BAV, BMVIT, IKSS, INTI, STRMTG

#Operators: Bayerische Zugspitzbahn,

Sommerbergbahn Bad Wildbad, Sandia Peak

Tramway, Zermatt Bergbahnen

Interested guests or new members with rope experience are welcome!



## Introduction of Study Commission (SC) II «Ropes»

ONTAF

Meetings usually 2 times per year

2018

Argentina | Berlin

2019

Winterthur | Garmisch-Partenkirchen

2020/21

online

2022

online | Stuttgart

2023

Oberstdorf



## Introduction of Working Group «Ropes»

Paper 28 / 2014

General recommendations for the manufacturers lubrication and the re-lubrication of steel wire ropes use in ropeway installations for Passengers

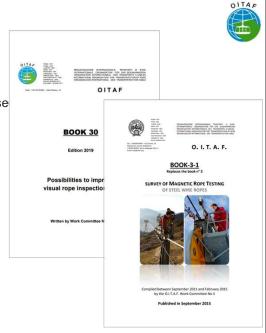
Paper 3-1 / 2015

Survey of magnetic rope testing of steel wire ropes

Paper 30 / 2019

Possibilities to improve visual rope inspection (VI)

Close to finishing and publishing: Ropelifetime



## **New Paper: Rope Lifetime**

\* Focus on Stranded Ropes \*

#### Basics about wire ropes used in ropeways

- Wire manufacturing, strand and rope designs
- Transport & assembly
- Rope end connections

#### Operational influences, e.g.:

- Vehicle clamps
- Rollers, sheaves
- drive, speed

#### Unscheduled influences, e.g.:

- twist, damage events, environment, heat, ...
- Special incidents out of experience of the group members







## **New Paper: Rope Lifetime**

#### **Degradation mechanisms**

Free rope length - fatigue, wear/abrasion, corrosion Splice and end connections - wear/abrasion, twist

#### Theoretical lifetime estimation by calculation

Lifetime estimation by Feyrer / University of Stuttgart Special Interest: lifetime estimation method of Leipzig

#### **Example Calculations**

**Discussion of Results** 







#### **Historical Introduction**

1834 Invention of the wire rope

1890-1920 Material ropeways by Bleichert & Co.

end 1920s First passenger ropeways

since  $\sim 1927$  Research / 1st bending-tests in Karlsruhe and Stuttgart

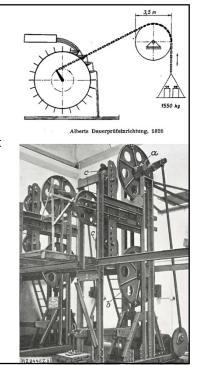
1936 Patent magneto-inductive rope testing

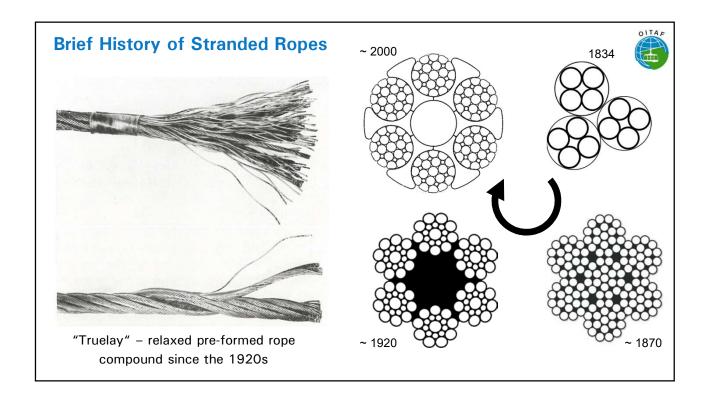
1980s First versions of Feyrer Formula

2000 + + Online monitoring, lifetime calculations

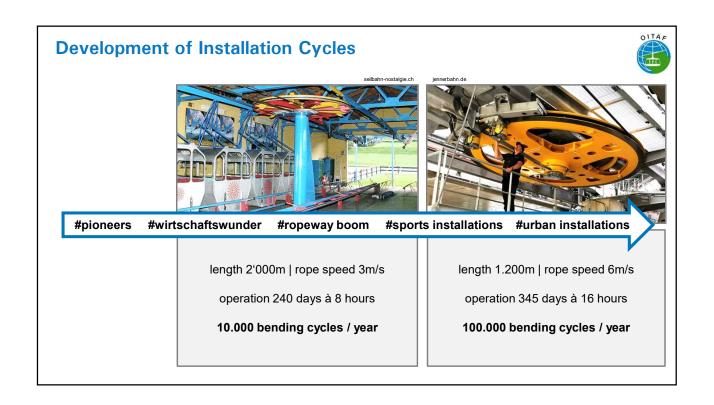
2005 European Standardization

Future Inspection Intervals based on bending cycles









## What is a Bending Cycle?





<u>Up to 5°</u> deflection: a rope can be considered as "not bended"

More than 5° deflection: rope takes the shape of the support element and has to be consideres as "bended"

Reverse bend & ~ 20° deflection: more damage





## **How to calculate Bending Cycles?**



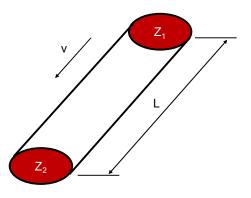
#### Example of a continuous moving monocable gondola

N	number	of	bending	cycles	per	vear	[-]
	Hallibol	$\circ$ .	bonanig	0,0100	POI	y ou:	LJ

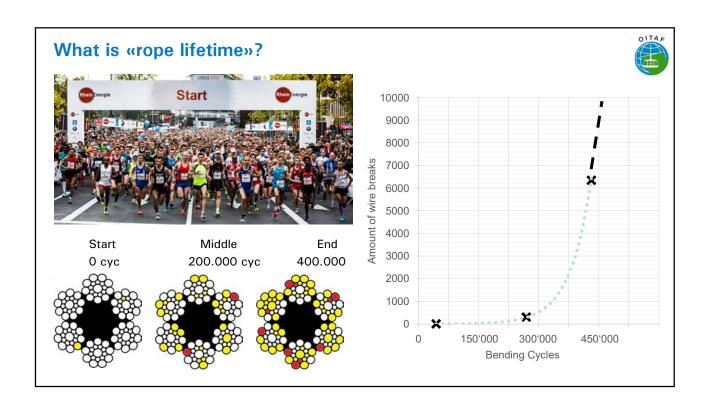
L length of the ropeway [m]

v nominal (usual) speed of ropeway [m/s] Z number of sheaves in the ropeway [-]

 $\begin{array}{ll} t_{\text{hours/day}} & \text{average operation hours per day [-]} \\ t_{\text{day/year}} & \text{average opertaion days per year [-]} \end{array}$ 



$$N = \frac{3600 \cdot v}{2 \cdot L} \cdot Z \cdot t_{hours/day} \cdot t_{days/year}$$



# What is «rope lifetime»? Ropes will develop fatigue, wear and possibly local damage within (long-term) operation Target: operate ropes as long as possible in safe conditions Limit: "discard maturity" – defined conditions under which a wire rope must be replaced Examples for point of discard • Local damage (which cannot be repaired any more) • Safe inspection is no more possible • Increase of wire breaks will be too fast for feasible future inspection intervals • development of wire breaks is not safely predictable We do not want to witness rope failures – we want to keep safe conditions and change a rope on time.

## «Overall package» of OITAF SC II Ropes



Visual Inspection
Magnetic testing
Lubrication
Rope lifetime management



- -> sustainable use of a rope
- -> planable maintenance actions
- -> preventive maintenance
- -> safe ropeway operation
- -> cost efficiency



Thank you for your attention!

Vielen Dank für Ihre Aufmerksamkeit!



Merci beaucoup pour votre attention!

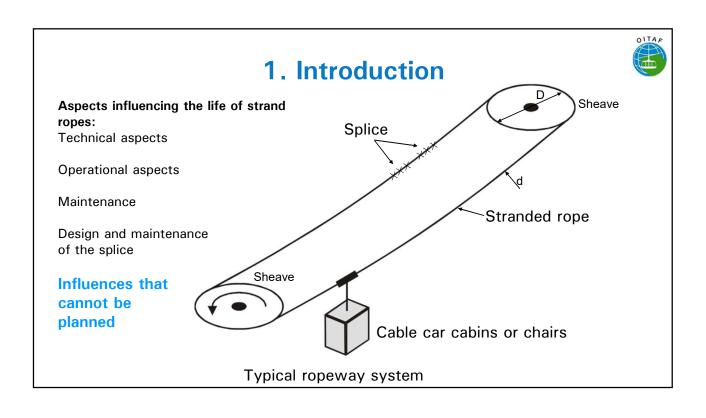
Grazie per la vostra attenzione!



# Operational aspects influencing the life of strand ropes



- 1. Introduction
- 2. Operational aspects over time
- 3. Rope installation
- 4. Influences during operation
- 5. Corrosion
- 6. Summary
- 7. Basics for a lifetime estimation (calculation)



# 2. Operational aspects over time



- · Within the last 20 years, ropes and their field application have developed rapidly
- Most important advantage of a rope is the fact that it reveals an upcoming damage early in time
- · If operators recognize the signs of damage, disasters are hardly possible
- Economic development was possible in terms of "bigger, faster, lighter, longer, more efficient, cheaper, etc."
- · Number of bending cycles is the main influence on the service lifetime of a rope

Development of number of bendings over the last decades and influence of parameters

Year	Installation Length [m]	Number of Sheaves	Max Speed [m/s]	Operation hours per day	Operation days per year	Max bendings per year	Increase Factor
1953	2390	2	2.5	7	120	3163	1
1999	932	2	5.5	8	270	45888	15
2010	805	2	6	18	365	176288	56
2022	2800	4	7.5	19.25	365	135506	43

# 3. Rope installation





 $\mbox{\bf Abrasion}$  - critical situation, rope too close to the soil



**Contact with obstacles** - disastrous situation

# During rope installation or during operation





Abrasion or crush of the outer wires of several strands



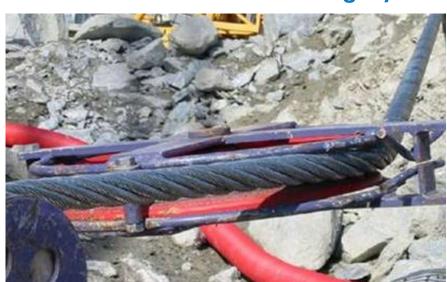




Improvised clamp missing groove unsmooth surface unknown sliding force

# Forced bending cycles





Deflection sheave kinging on a diverting sheave caused by insufficient orientation of the sheave



# 4. Influences during operation

**Differences in rope tension forces** lead to changes in the lay length, in torque and twist, but also to different transverse forces. Fatigue and abrasion may occur.

#### Expected different rope tension results from:

- Height difference bottom station mountain station (haulage rope)
- · Difference of rope tension before drive wheel after drive wheel
- Load condition
- Dynamic forces from acceleration / deceleration
- Meteorological influences (temperature, wind, ice, etc.)

**Unexpectedly fast changes** may occur from heavy storm with gusts, ice shedding, trees fall on ropes, etc.

It is important to remember not to constantly change the driving speed. A constant driving speed protects the system (oscillations / vibrations) and the rope.

and

The energy in the system dependents quadratically from the driving speed.

# OITAF

# **During operation, grips**



# **Damage** caused by fixed grips after a too late relocation

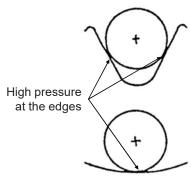


**Negative imprint** of the rope in a fixed grip

Running on rollers and sheaves







Small lining grooves lead to wear at the edges and to twisting

Ropeway drives using a double grooved traction sheave and a counter sheave with different diameters lead to wrapping tension, further unequal abrasion and high stresses in the rope

# Running on rollers and sheaves





Running ropes should only touch the soft inserts of rollers, wheels, supports and the clamps

Other contact, with any hard construction elements or flanges of rollers can damage the rope massive

Roller Damages seriously damage the rope



# **Environmental influences, Lightning strikes**



**Lightning strikes**not predictable
Not reliably detectable by MRT
recognisable by visual inspection

# Environmental influences, Heat on rope





Heat impact on a carrying-hauling rope

#### Heat of fire

damages the outer wires starting at about 200°C

Failure of the core means that the rope compound loses its support leading to touching strands, wear, corrosion and wire breaks

Lubricants can melt from about 60°C or even lose their properties at about 100°C

Ropes should be kept in motion to prevent local rope sections from heat damages

After exposure to heat on ropes, it is essential that they are assessed by competent persons

# **Environmental influences, Heat on structures**





#### Heat from sunlight

towers are prevented from heating up by installing sheet-metal panels covering the shafts

#### Melting of permafrost

leads to deformations, settlements and thus to dis-alignments of the track, to twisting and different lay length, up to rope derailment

Melting of permafrost under drive stations To protect the permafrost from warming up, foundations are specially insulated against the subsoil to prevent disalignments of the track

# **Derailment and rollovers**





Rollover of a hauling rope

#### Rollover of hauling rope

Rollovers can be caused by vibrations due to emergency braking or wind.

Both track rope and hauling rope should at least be visually inspected after such an incident.

Derailments of funicular ropes can happen quite often.

Especially for concave slope designs, in combination with transverse wind, the rope can fail to lay back into the track rollers.

If derailments mainly happen in the passing loop, the rollers may be insufficiently adjusted or worn. In this case, the rope can be damaged over a very long distance.

In any case of derailment, a competent person should be consulted.



# Environmental influences, electrical fields



Moving rope in electromagnetic field generates electrostatic charges of the rope.

At electrically earthed points of contact with the rope, the wires may locally overheat.

Increased wire fracture and reduced lifetime of the rope are the results.

#### Conclusion

No ropeways near high-voltage powerlines and transmitter-masts.

As a rule, the ropeway control reacts more sensitively than the rope...

# Environmental influences, volcanic ashes







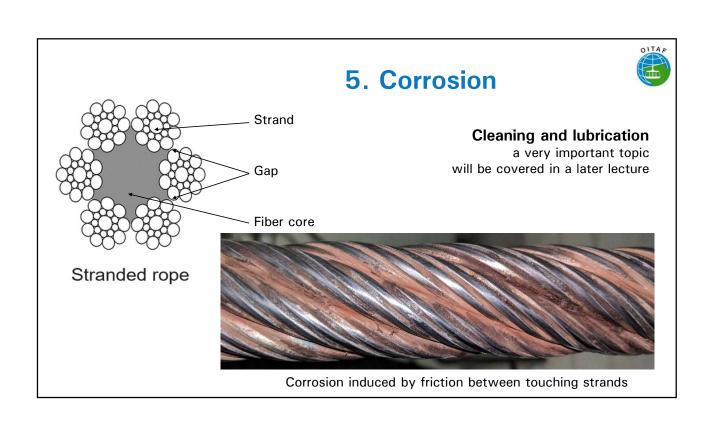
#### After volcano eruption

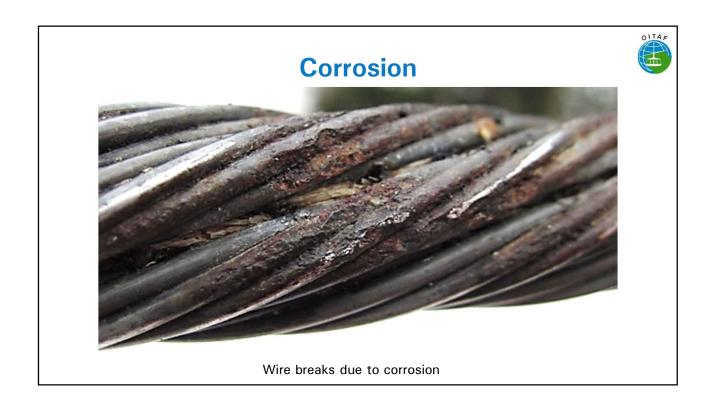
Ropeways in the vicinity of volcanoes are very exposed to atmospheric influences such as carbon, sulfur, salt water, etc.

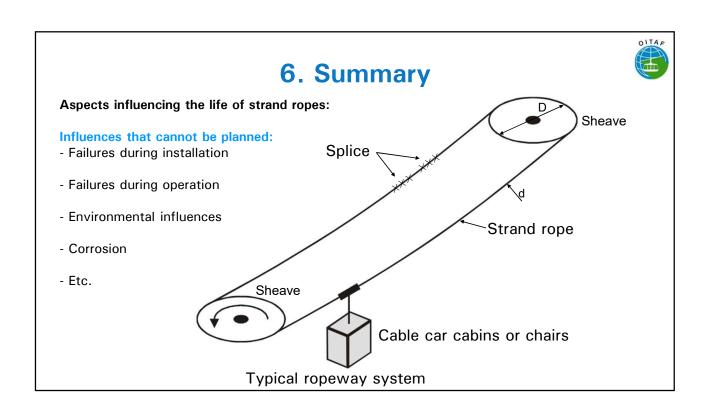
Bright ropes instead of galvanized ropes In this specific environmental condition, the bright ropes shall be advised in respect to the galvanized ropes. In fact, the released sulfur vapors are able to connect with the zinc and create a brittle structure that result in a premature and fast rope failure.

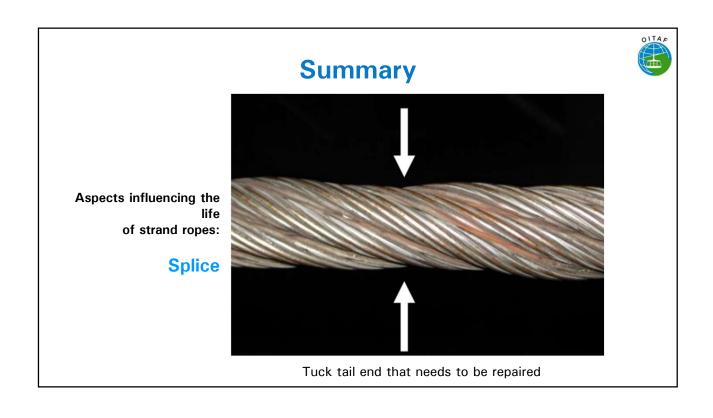
#### Rope after volcano eruption

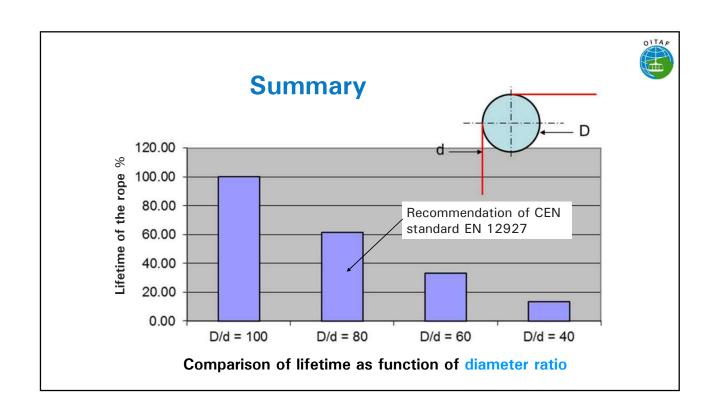
Without cleaning, the lifetime of the rope is greatly reduced

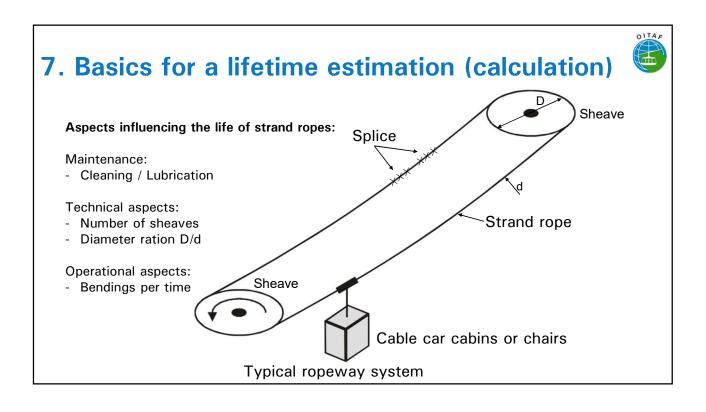


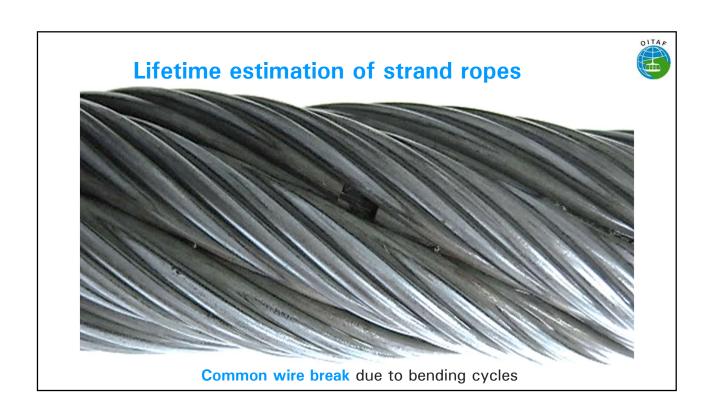


















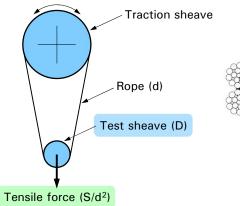
3. Lifetime Estimation "Feyrer Method"

# Life time estimation formula



Formula of Prof. K. Feyrer from IFT, University of Stuttgart

$$lgN = b_0 + \left(b_1 + b_3 \cdot \lg\left(\frac{D}{d}\right)\right) \cdot \left(lg\left(\frac{S}{d^2}\right) - 0.4 \cdot lg\left(\frac{R_0}{1770}\right)\right) + b_2 \cdot lg\left(\frac{D}{d}\right) + lg(f_d) + lg(f_L) + lg(f_E)$$





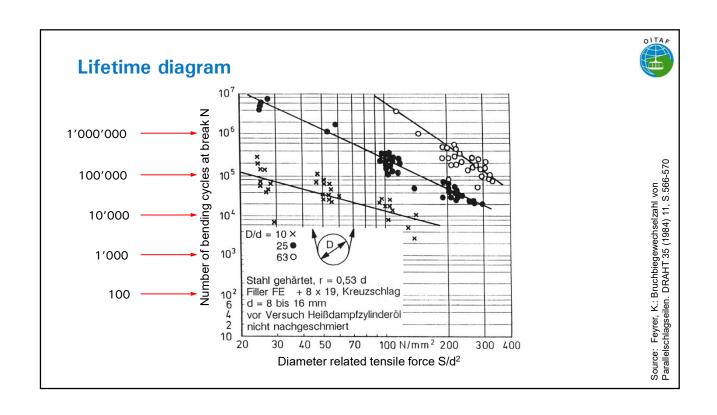
Life time estimation – Bending over sheave test

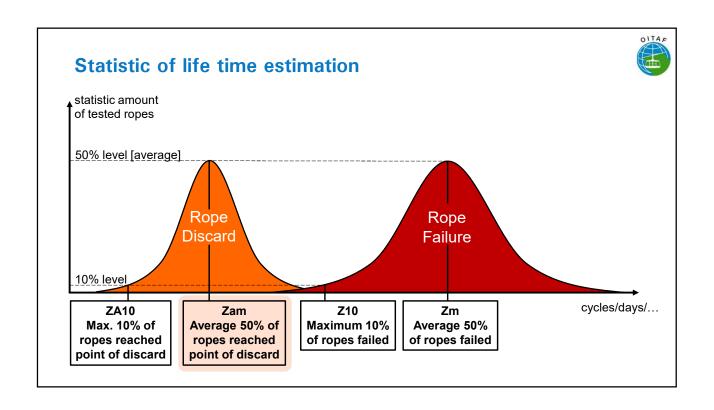






Source: IFT, University of Stuttgart





# OITAR

#### Life time estimation formula

$$lgN = b_0 + \left(b_1 + b_3 \cdot \lg\left(\frac{D}{d}\right)\right) \cdot \left(lg\left(\frac{S}{d^2}\right) - 0.4 \cdot lg\left(\frac{R_0}{1770}\right)\right) + b_2 \cdot lg\left(\frac{D}{d}\right) + lg(f_d) + lg(f_L) + lg(f_E)$$

The formula is valid with following requirements

- · Single bending
- · Round steel groove
- Groove radius r = 0.53d
- · No side deflection of the rope
- · Rope generously lubricated with heavy oil or vaseline
- · In dry rooms

#### Results:

- Z<sub>m</sub>: Average 50% of ropes broken
- Z<sub>10</sub>: Maximum 10% of ropes broken
- $Z_{\text{am}}$ : Average 50% of ropes reached point of discard
- Z<sub>a10</sub>: Maximum 10% of ropes reached point of discard



## Correction factors F<sub>N</sub>

Factors  $f_N$  for adapting the calculated values of bending cycles to the real conditions

$$N_{korr} = N \cdot f_{N1} \cdot f_{N2} \cdot f_{N3} \cdot \cdots \cdot f_{Ni}$$

- $f_{N1}$ : Rope lubrication
  - Rope well lubricated: 1.0
  - Rope without lubrication: 0.2
- $f_{N2}$ : Side deflection
  - · Not applicable for ropeways
- $f_{N3}$ : Groove material
  - Steel: 1.0
  - Plastic / Polyurethan:  $f_{N3} \approx 0.75 + 0.36 \cdot \frac{S/d^2}{D/d} 0.023 \cdot \left(\frac{S/d^2}{D/d}\right)^2$

Example for  $f_{N3}$ :

- Low load: 1.01

- High load: 1.24

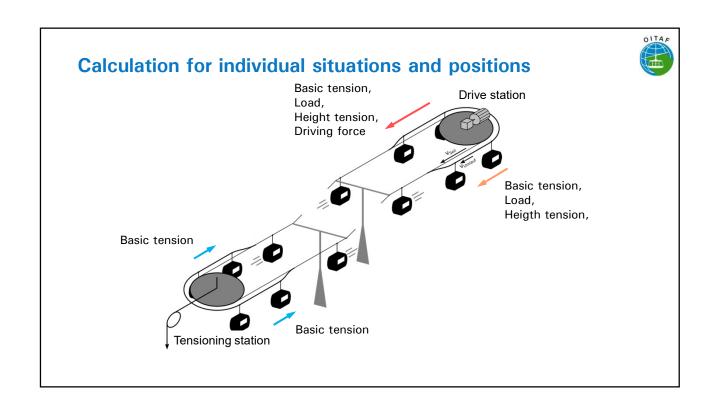


# Factor for rope tensile force

Rope tensile force can vary:

$$S = \frac{Q \cdot g}{n_T} \cdot f_{S1} \cdot f_{S2} \cdot f_{S3} \cdot f_{S4} \cdot f_{S5} \cdot \cdots$$

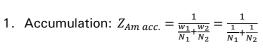
- $f_{S1}$ : Friction in rope drive (roller guide / sliding guide)
- $f_{S2}$ : Efficiency of the rope
- $f_{S3}$ : Parallel ropes
- $f_{S4}$ : Speed / Acceleration
- f<sub>S5</sub>: Bending with changing tensile force



# Accumulation of separate lifetime values

Palmgren-Miner Formula:

$$Z = \frac{1}{\sum_{N_i}^{w_i}}$$



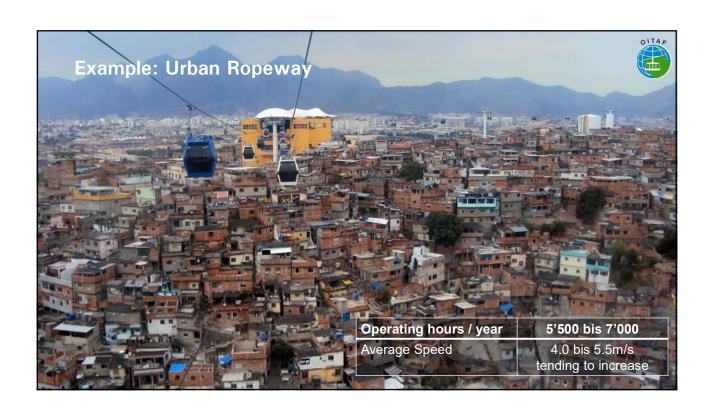
Working cycles accumulated over 2 sheaves for one operation mode

2. Accumulation:  $Z_{load} = \frac{1}{\frac{w_1}{N_1} + \frac{w_2}{N_2}} = \frac{1}{\frac{x\%}{N_1} + \frac{y\%}{N_2}}$ 

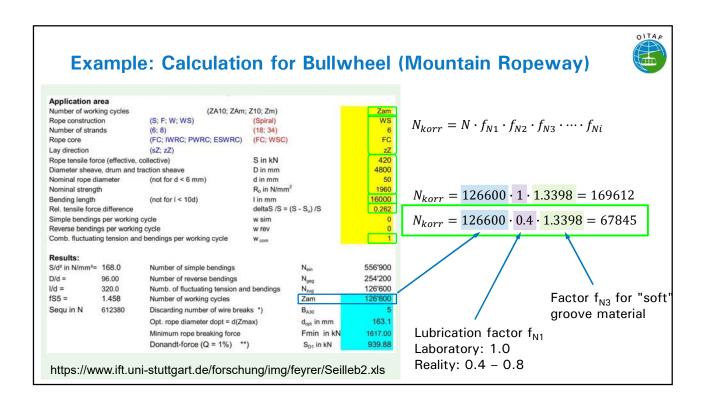
Accumulated working cycles with accumulated portion of operation modes







Exam	ole for Calculation		Per la
L	4000 m	L	4000 m
ΔΗ	600 m	ΔΗ	50 m
V	4.5 m/s	v //	5.5 m/s
d	50 mm	d	50 mm
D	4800 mm	D	4800 mm
Bull wheel	Phipe u Patter	Bull wheel	THE REPORT OF THE
F1 💃	420 kN	F1	420 kN
F2	310 kN	F2	330 kN
ΔS/S	0.262	ΔS/S	0.214
FN3	1.3398	FN3	1.3398
Return wheel		Return wheel	2 7 1
F1 = F2	190 kN	F1 = F2	320 kN
ΔS/S	0	ΔS/S	0
F <sub>N3</sub>	1.0168	F <sub>N3</sub>	1.1993



## Accumulation for lubrication factor 1.0



Mountain Ropeway

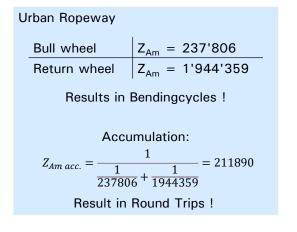
Bull wheel 
$$Z_{Am} = 169'612$$

Return wheel  $Z_{Am} = 12'781'376$ 

Results in Bendingcycles!

$$Z_{Am\ acc.} = \frac{1}{\frac{1}{169612} + \frac{1}{12781376}} = 167391$$

Result in Round Trips!



### Accumulation for lubrication factor 0.4



#### Mountain Ropeway

Bull wheel 
$$Z_{Am} = 67'845$$
  
Return wheel  $Z_{Am} = 5'112'551$ 

Results in Bendingcycles!

$$Z_{Am\ acc.} = \frac{1}{\frac{1}{67845} + \frac{1}{5112551}} = 66956$$

Result in Round Trips!

#### **Urban Ropeway**

Bull wheel 
$$Z_{Am} = 95'122$$
  
Return wheel  $Z_{Am} = 777'744$ 

Results in Bendingcycles!

#### Accumulation:

$$Z_{Am\ acc.} = \frac{1}{\frac{1}{95122} + \frac{1}{777744}} = 84756$$

Result in Round Trips!

#### Result in time



Round trips per year = 
$$\frac{\mathbf{t} \cdot \mathbf{d} \cdot \mathbf{v} \cdot 3600 \frac{s}{h}}{L}$$

- t: Operating hours per day
- d: Operating days per year
- v: Operating speed [m/s]
- L: Length of rope loop [m]

$$Lifetime in years = \frac{ZAm \ accumulated}{Round \ trips}$$

#### Result in time



Mountain Ropeway

t: 10 hours per day

d: 120 days per year

v: 4.5 m/s L: 4000 m

Lifetime

Lubrication Factor 1: 34.4 years

Lubrication Factor 0.4: 13.8 years



#### **Urban Ropeway**

t: 18 hours per day

d: 350 days per year

v: 5.5 m/s L: 4000 m

Lifetime

Lubrication Factor 1: 6.8 years

Lubrication Factor 0.4: 2.7 years



## **Learnings**



What is it good for?

- Useful method for service life estimation
- Optimisation of rope drives
- Evaluation of changes, for example during a rebuild project
- Service life estimation as a basis for determining or adapting inspection intervals
- Service life estimation as a supplement to the results of the MRT

Important: Standards only specify the maximum permissible inspection interval. In case of high utilisation, this interval must be shortened!







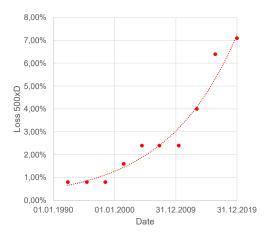


1. Evolution of Damage in Wire Ropes

# **Evolution of Damage in Wire Ropes (example)**



Date	Broken wires	Loss 6xD	Loss 30xD	Loss 500xD
26.12.2019	155	1.6%	4.7%	7.1%
10.6.2016	121	1.6%	1.6%	6.4%
4.6.2013	102	1.6%	1.6%	4.0%
17.6.2010	83	1.6%	1.6%	2.4%
25.4.2007	60	1.6%	1.6%	2.4%
15.6.2004	44	1.6%	1.6%	2.4%
26.6.2001	25	0.8%	0.8%	1.6%
15.6.1998	13	0.8%	0.8%	0.8%
20.6.1995	5	0.8%	0.8%	0.8%
5.5.1992	1	0.8%	0.8%	0.8%



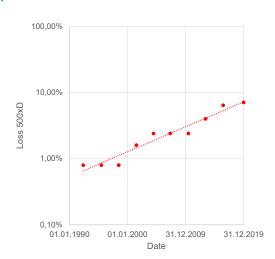
# Semi-logarithmic Diagram



#### Evolution of damage is more or less exponential

A linear trend line approximates the evolution of damage (data from slide 3)

- The trend line in general does not go through an experimental point
- Predictions based on the trend line are not conservative
- and should not be used for safetyrelevant predictions (as for example the latest safe date for the next MRT inspection)





# 2. Principles of Safe Prediction



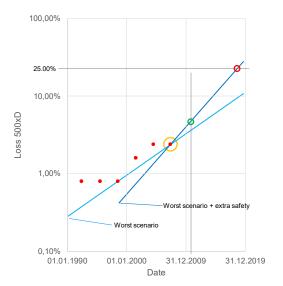
## **Principles of Safe Prediction**

- The prediction should start at the current point
- The prediction should reflect the worst scenario imaginable
  - (whatever that means)
- Damage mechanisms may change over time
  - A prediction should take this into account in an appropriate way.
- The loss of cross-section is difficult to predict, it may be necessary to couple it to the evaluation of the number of broken wires
  - The loss of cross-section tends to be proportional to the number of broken wires
  - · In the case of few wire breaks, this assumption is on the conservative side

# **Graphical execution of the prediction**



- Yellow circle: Starting point
- Draw a line trough the last measurement reflecting the worst scenario
- Draw a second line with increased slope
  - by a safety factor, your experience
- Green circle: Next MRT due to legal requirements
- Red circle: End of life
- Choose the due date of the next MRT
  - · due to egal requirements or
  - · before end of life,
  - · what ever occurs first
- Don't use the 40% limit on 500xD for predicions of the latest safe MRT due date



## Excel & Co.



- The whole method can be implemented with spreadsheet apps
  - · The kernel Excel function of the method is LINEST
    - · RGP in German
    - · DROITEREG in French
    - · REGR.LIN in Italian
  - Help says: «The LINEST function calculates the statistics for a line by using the "least squares" method to calculate a straight line that best fits your data, and then returns an array that describes the line. You can also combine LINEST with other functions to calculate the statistics for other types of models that are linear in the unknown parameters, including polynomial, logarithmic, exponential, and power series. Because this function returns an array of values, it must be entered as an array formula.»
  - · You may need to calculate the slope of the regression line as well as its standard deviation
  - · You must take into account your personal experience in the form of a safety factor



# 3. Practical application

# Application to example (data from slide 3)

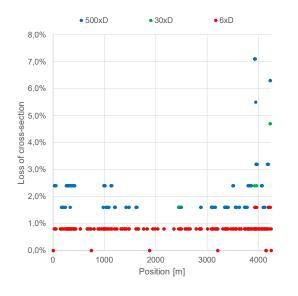


Date	Broken wires	Prediction broken wires	Loss 6xD F	Prediction 6xD	Loss Pr 30xD	ediction 30xD	Loss P 500xD	rediction 500xD
26.12.2019	155	191	1.6%	2.5%	4.7%	2.5%	7.1%	10.3%
10.6.2016	121	162	1.6%	2.5%	1.6%	2.5%	6.4%	6.4%
4.6.2013	102	144	1.6%	2.8%	1.6%	2.8%	4.0%	4.2%
17.6.2010	83	123	1.6%	3.3%	1.6%	3.3%	2.4%	4.9%
25.4.2007	60	99	1.6%	3.6%	1.6%	3.6%	2.4%	5.4%
15.6.2004	44	72	1.6%	2.3%	1.6%	2.3%	2.4%	4.6%
26.6.2001	25	54	0.8%	3.3%	0.8%	3.3%	1.6%	3.3%
15.6.1998	13		0.8%		0.8%		0.8%	
20.6.1995	5		0.8%		0.8%		0.8%	
5.5.1992	1		0.8%		0.8%		0.8%	

# Remarks on the example (slide 3)



- The broken wires in the most-damaged region were visible
- The operator repaired the rope in this region after the rope inspection of the 26.12.2019
- The results of later MRT's are not shown here, because they are no longer comparable
- The distribution of the rope damage on the 26.12.2019 is shown in the diagram





# 4. Conclusions

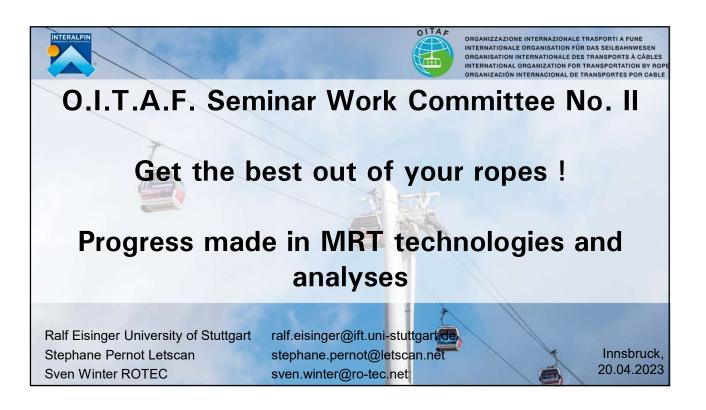
# OTTAF

■ Pro's:

**Conclusions** 

- · We have 20 years of experience with predictions based on MRT results
- · The method safely predicts the evolution of damage over one MRT period
  - We have only a few MRT results exceeding the prediction (< 1 / year with 500 MRT / year)</li>
- · The method is very powerful in estimating safe MRT periods
- · The method handles the distribution of damage correctly
- Con's:
  - · Implementation in Excel is complex and error-prone
  - The quality of the prediction decreases with reference length
  - The predictions for the reference length 6xD are not very reliable





# What is MRT? • The rope is strongly magnetised • Due to the rope structure, a so-called basic signal is then formed • Deviations from this rope structure then show up as pecularities in the course of signal

# **Technical aspects**



Magnetic field generation

- · Permanent magnet
- Electromagnet

#### Sensors

- · (Classical) coil
  - · Change of magnetic field
  - · Speed dependent
- Hall effect sensors
  - · Absolute value of the magnetic field

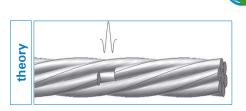
# **Analysis methods**

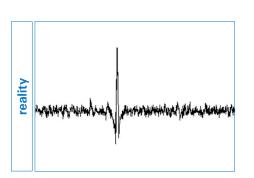
Typical analysis methods

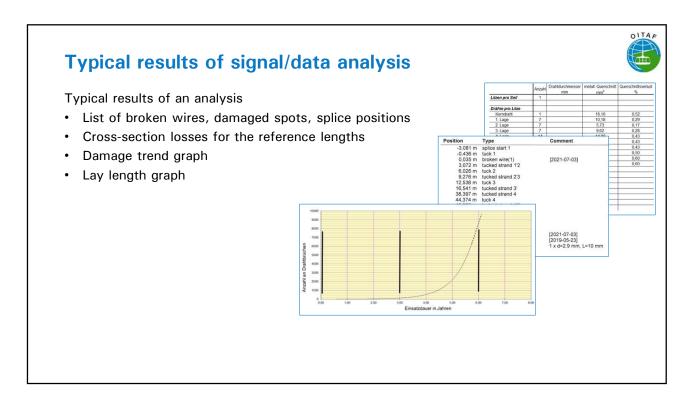
- · Manual analysis
- Automatic analysis
- · Comparative analysis

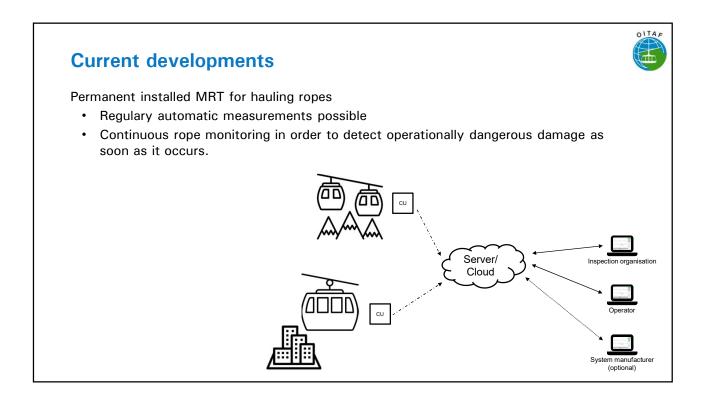
Examples of mathematical methods:

- · classic peak detection
- FFT (Fast Fourier transformation)
- Wavelet
- · Fuzzy method









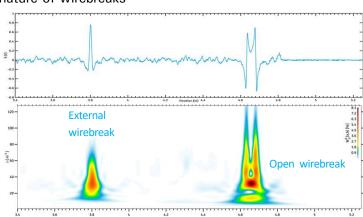
# OLTAF

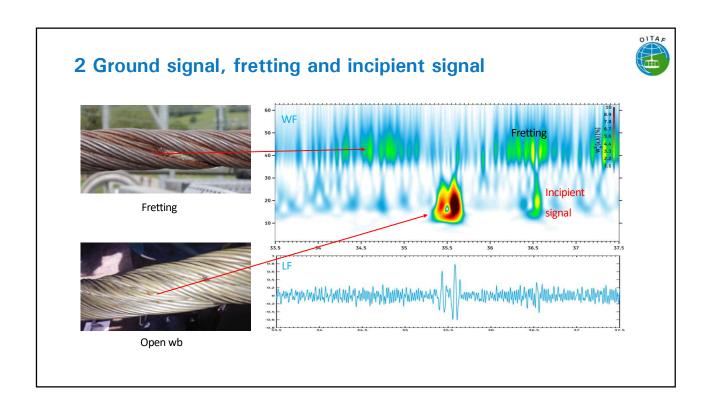
# 2. Assessing rope damage with Wirelets

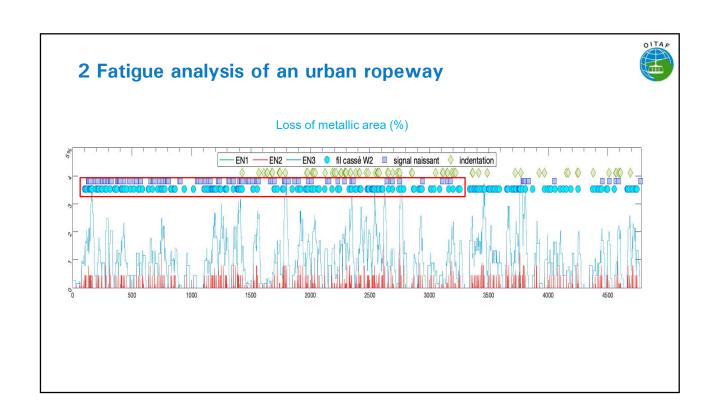
- Wirelet scalogram of magnetic signals
  - · Time-frequency representation of signal energy
  - · Concept of instantaneous frequency

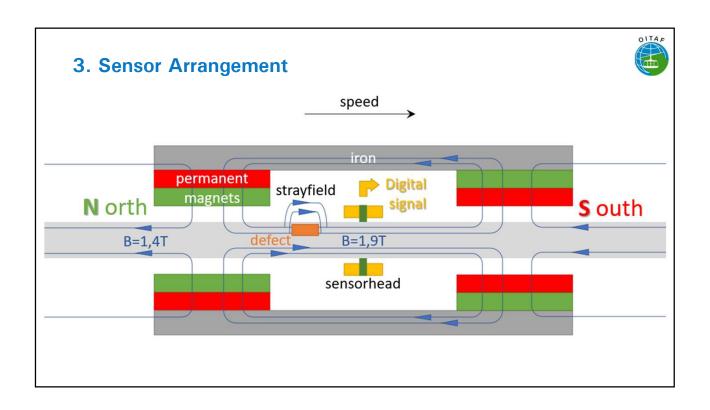
$$W_{\Psi}^{s}(a,b) = \frac{1}{\sqrt{a}} \int_{-\infty}^{+\infty} s(x) \overline{\psi\left(\frac{x-b}{a}\right)} dx$$

• Wirelet signature of wirebreaks













- Multi channel sensor concept:
  - Up to 48 Hall sensors individually scanned (rope enclosing)
  - 2 induction coils



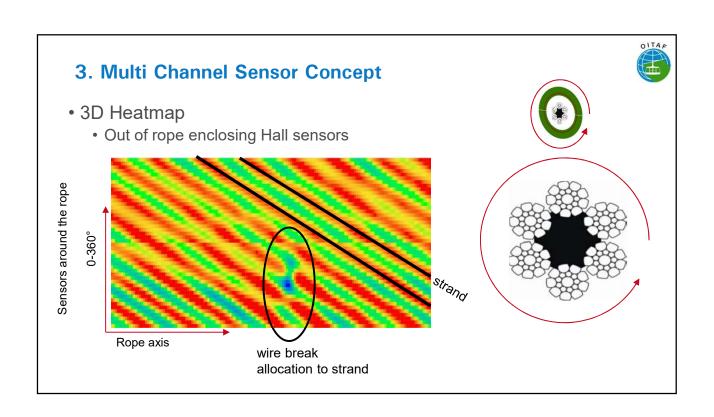
- 5 outputs:
  - 2 LF channels: LF 1 & LF 2
  - Hall LF channel
  - LMA channel
  - 3D heatmap

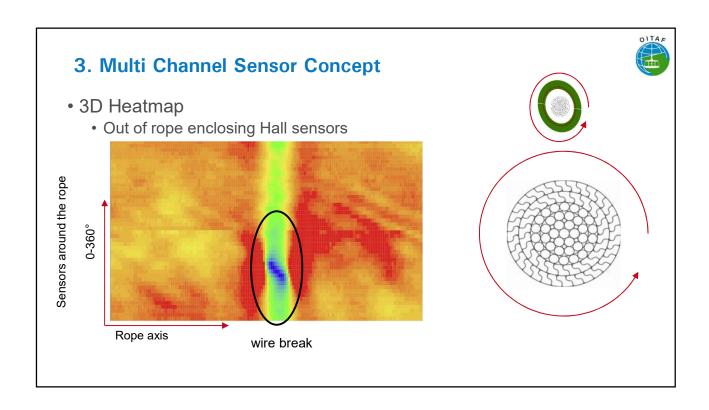


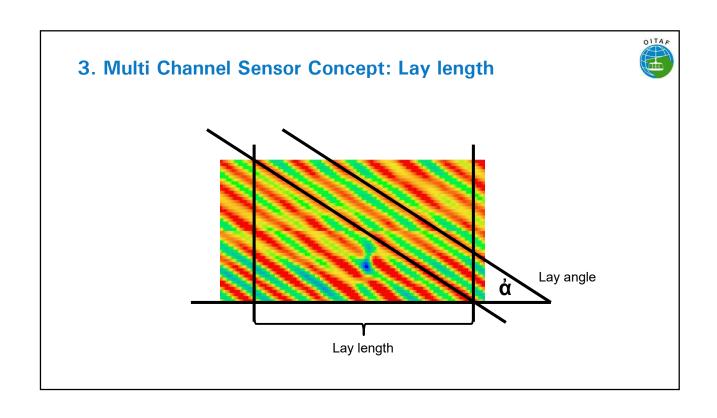
# 3. Multi Channel Sensor Concept

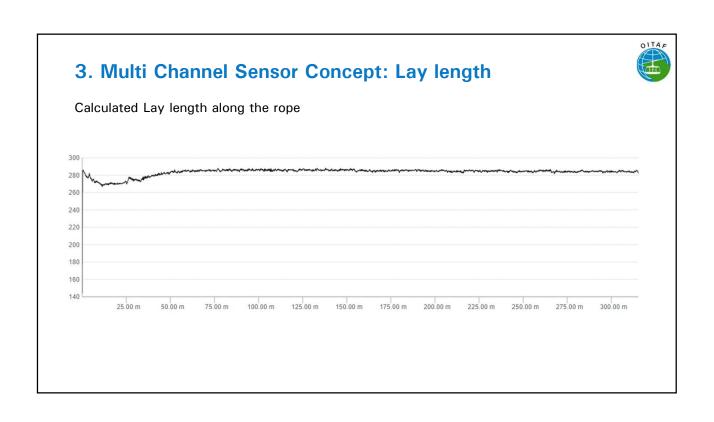


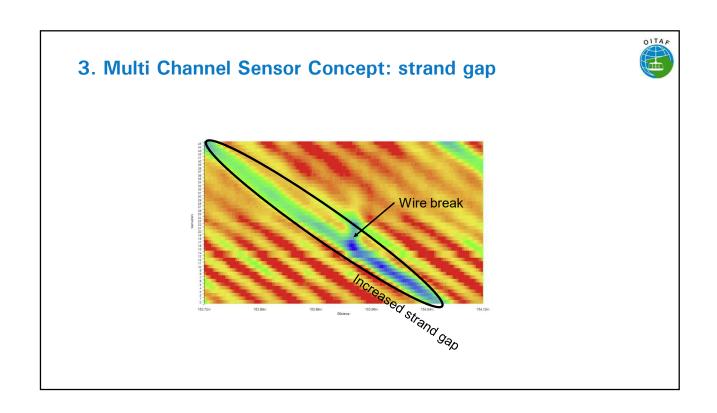
Channel	LF 1 & LF 2	Hall LF	LMA	3D Heatmap
type	Induction coils	Hall sensors	Hall sensors	Hall sensors
		0	0	0
category	Local Fault	Local Fault	Loss of Metallic Area	Local Fault
Type of defect	Broken wires (Wear, corrosion)	Broken wires (Wear, corrosion)	Wear, Corrosion	Broken wires geometry faults (lay length…)
Advantage	Redundancy: Inde	pendent Channels	absolute value	3D representation Location info
Min. Speed	0,3 m/s	0 m/s	0 m/s	0 m/s





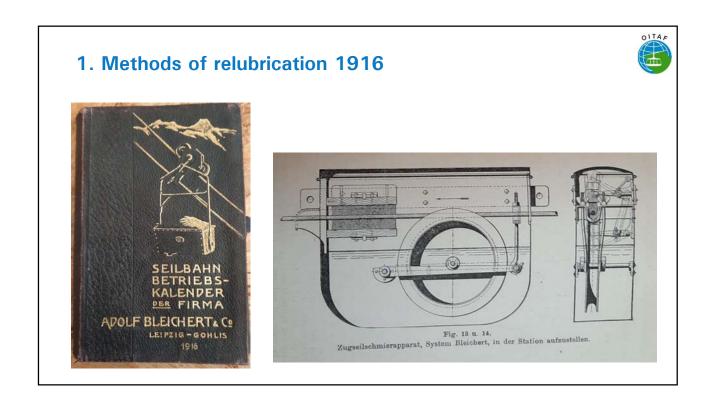








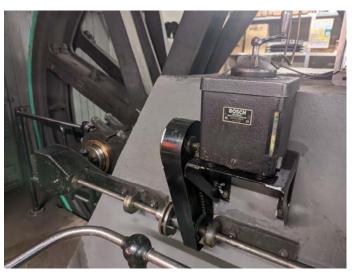




# 1. Methods of relubrication 1929



Mechanical Oiler from 1929 at funicular in Stuttgart



# 1. Chair Lift





Source: www.wikipedia.org

# 1. Ungalvanized rope 1950







# 1. Galvanized rope 1960

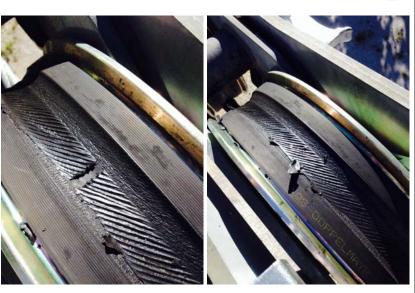


Since the 1960s, galvanized ropes became more and more common.

Corrosion was no longer a problem

Due to the contamination of the ropeway and passengers, the primary lubricant and relubrication were increasingly reduced or neglected.

Rope lubrication got a negative image



# 1. Galvanized rope 1960

Due to unsuitable relubricant, the roller rubbers were dissolved and damaged.

As a result, a large number of the track rollers had to be replaced prematurely.

For this reason, the operators have significantly reduced or completely stopped relubrication.





# 2. Lack of basic lubrication in today's haulage ropes

Very low basic lubrication for a new rope



At rope opening after 4 years of operation



After two years of operation, there is already significant corrosion on the strands





# 3. Primary lubrication and relubrication requirements

#### Primary lubrication:

- Uniform distribution of the lubricant during stranding
- For good basic lubrication, approx. 30 g/sq. m. of wire surface should be applied.
- For a 40 mm rope (rope weight 6kg/m), it is approx. 75 g per meter of rope

#### Relubrication:

- Relubrication should be frequent or permanent during operation
- The relubricant must be compatible with the base lubricant
- The relubricant should be creepable so that it reaches the inside of the strand.
- The relubricant must be compatible with the roller rubbers

#### 4. Rope lifetime and amount of lubrication 14,0 Rope discard criteria 12,0 90 liter per 100m rope 80 10,0 70 Discard criteria in 8,0 60 6,0 50 40 30 2,0 20 0,0 10 10 rope diameter in mm 300000 400000 500000 600000 700000 800000 900000 less relubrication poor lubricated rope 10g/qm (standard today) medium relubrication Well lubricated rope 30g/qm ---much relubrication ■Well lubricated rope 30g/qm and relubricated

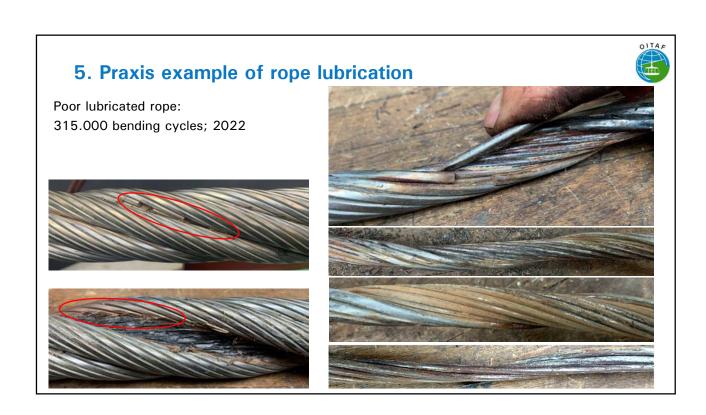
40

# 5. Praxis example of rope lubrication

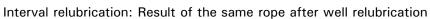


Poor lubricated rope: 0 bending cycles; 2017





# 6. Methods of relubrication













# 6. Methods of relubrication

Permanent oiling dependent on rope speed

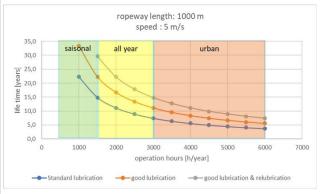


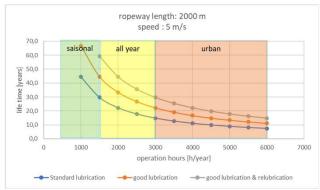




# 7. Rope lifetime and costs depending on lubrication incl standard = 10 g/m2 lub., good = 30 g/m2 lub







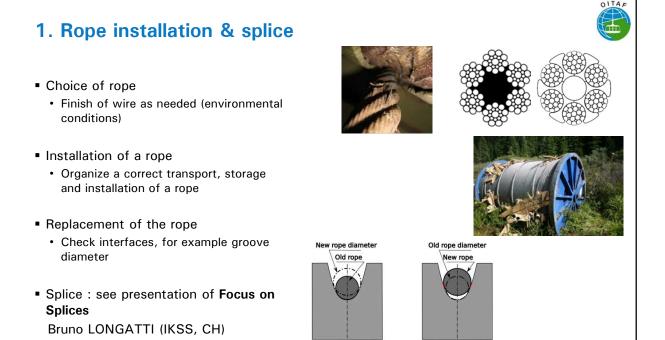
Rope cost: 500.000,- EUR; Standard lubrication: life time 10 years

4000m rope; 300day a 10h Rope Cost: 50.000,- EUR/year

Relubrication: life time 20 years Rope Cost: 25.000,- EUR/year







# 2. Operation/Maintenance

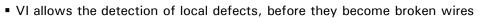


- Consider sustainable rope operation parameters:
  - · Speed of operation
  - · Avoid unnecessary cycles
- Following other components of installation
  - · Alignment of line
  - Follow state of lining of sheaves and rollers (see slide 1)
  - · Follow state state of grip
  - · Relocate fixed grips





# 3. Use VI



• Immediately after a known event, as derailments, clamp sliding, etc.;

You can take actions before, by grinding surface in some case for example:









# 3. Use VI

- VI allows the detection of local defects, before they become broken wires
  - At the normal periodicity for undetected event, as lightning strikes, scratches and notches, for examples.

You can take actions before, by grinding surface in some case for example:



# 4. Use MRT



- MRT allows to follow:
- Development of wire breaks;
- · Density of local damage accumulation;
- Select the right MRT periodicity for next test.
   (see presentation of Service life predictions based on MRT in practice, Stefan MESSMER (IWM AG, CH))

You can take actions on maintenance, for example on relubrication, or programme repair, by strand replacement or a complete section of a rope

Both VI and MRT informations allow to renew the rope in time before it is too late



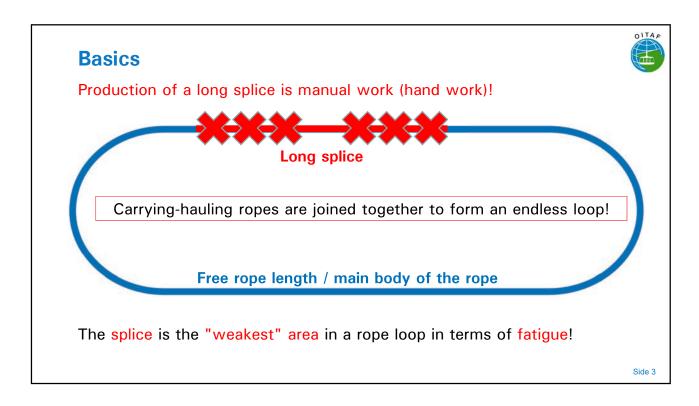


# Content themes about a long splice



- **Basics**
- > Functionality of a long splice
- > Execution of a long splice
- Discard criteria's
- > Knowable damages on splices
- Maintenance
  - Inspection + Servicing
  - Shortening
  - Repair within splice length
  - Repair in the free rope length
- > Splice and Rope lifetime
- **➤ History / Future**







# Basics Long splice acc. EN 12927 Tucked tails

Tuck: location in a splice where 2 opposite outer strands of a rope enter into the core

→ At least as many tucks as strands

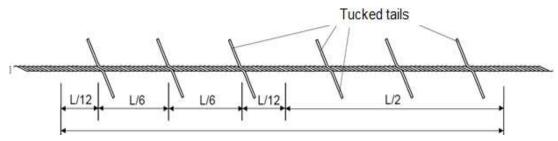
Tucked tail: area in a splice where 1 outer strand (properly wrapped) replaces the rope core

→ At least twice as many tuck tails as strands

Side 5

# **Basics / Hazard scenarios**





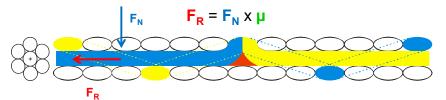
Long splicing of 6 strand haulage, carrying-hauling and carrying-hauling ropes for ski-tow:

- the risk of deformation and slipping of the spliced rope ends may be reduced by a correct correlation of geometrical characteristics of the two ropes connected by the splice, by selecting the splice geometry in accordance with this standard and by selecting the correct auxiliary (wrapping) material;
- > the risk of an insufficient attachment of the grip to the rope may be reduced by applying limitations to the diameter of the splice in accordance with this standard;
- Diameter reduction in the splice area may lead to an increase of stresses in the rope.

# Functionality of a long splice



Frictional connection between the strands surrounding the rope, the winding material and the inserted strand





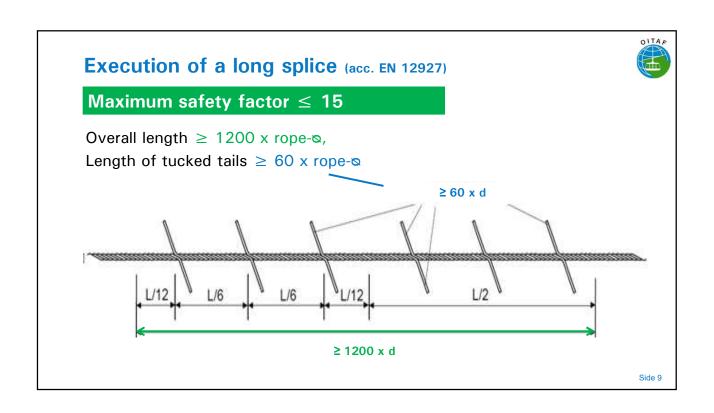
- $\blacktriangle$   $F_N$  dependent on:
  - Rope tension
  - Winding angle
- ▲ F<sub>R</sub> dependent on:
  - $-F_N$
  - $-\mu$  Friction coefficient of friction between outer strands wrapping material inserted strands

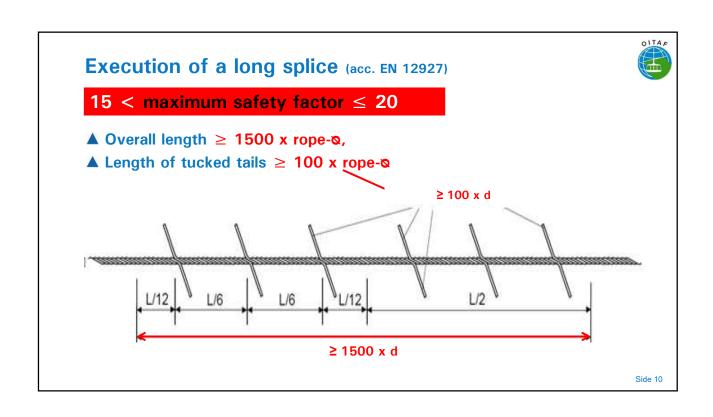
Side 7

# **Execution of a long splice (acc. EN 12927)**



Variables:	Recommendations:	
Total length of a long splice	> = 1200 or 1500	
Length of tuck tails	> = 60 or 100	
Diameter of tucks whole splice area	< = +8% (10%) of nominal Ø > = -10% of nominal Ø	
Waviness within the splice area	< 6% of nominal Ø	
Splice version	no requirements	
Wrapping material of the tuck tails	no requirements	
Splice tucks execution type	no requirements	
Type of splice tuck supports	no requirements	
Type and design of the inserts	no requirements	



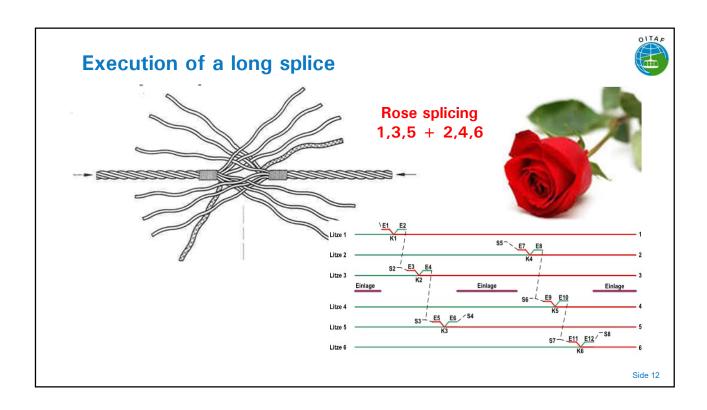


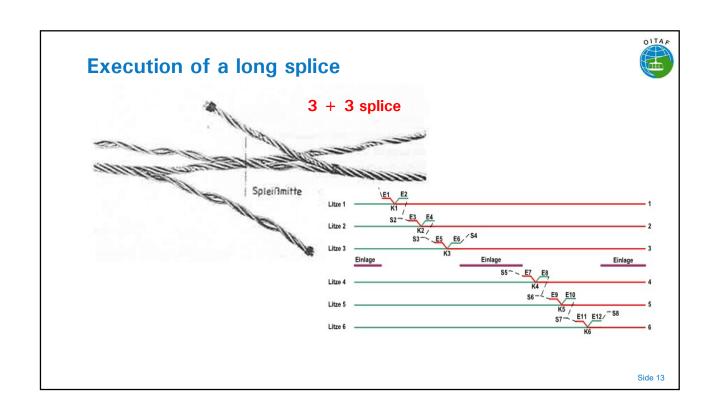
# OITAR

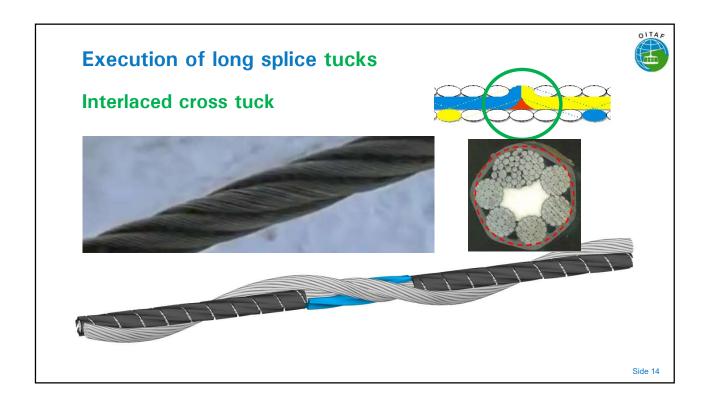
# **Execution of a long splice**

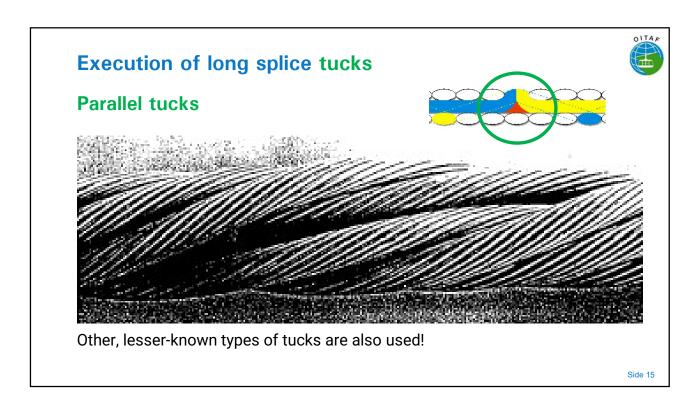
# Standard specifications according EN 12927

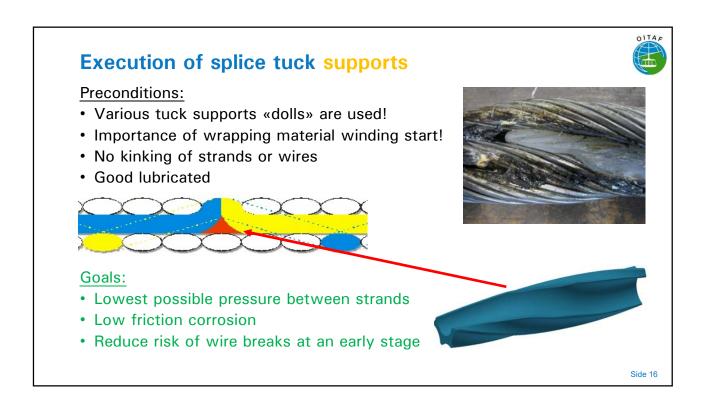
- ➤ The tensile safety of the rope does not exceed 20 in the splice area and is not less than the values set out in EN 12930.
- ➤ Splicing shall be performed by a skilled person, the "splicer", following a written procedure. The splicer shall have knowledge and practical experience and shall be capable of assessing the quality of the splice in relation to the requirements of this standard.
- > The rope splice shall not contain any added magnetic material.
- ➤ If there are two or more splices, they shall be properly recognizable and they shall be traceable by means of the splice documents.











# **Execution of the tuck tail wrapping**

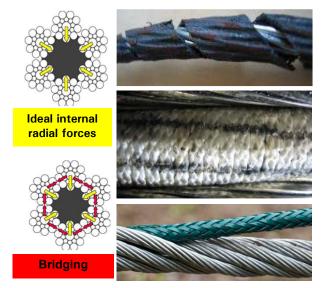
# ONTAR

# Preconditions:

- Various wrapping materials are used for doubling up the inserted tuck tails and creating friction
- Wrapping material is durable, flexible

# Goals:

- Preventing metallic contact between the inserted tuck tails and the outer strands
- Reduce risk of fretting and wire breaks at an early stage



Side 17

# **Execution core portion between tuck tail ends**

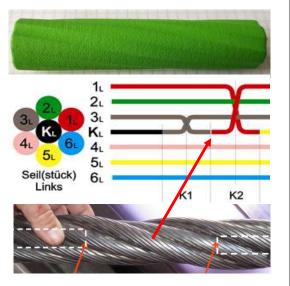
# Preconditions:

- Various inserts are used!
- · Diameter of the inserts is big enough
- · Insert is durable
- Tuck tail ends are close to each other or to the insert

#### Goals:

- Reduce risk of shrunken tuck tail ends
- Reduce risk of fretting and wire breaks at an early stage

Attention: Damages at tuck tail ends are difficult to repair!





# Discard criteria's for long splices (acc. EN 12927)

#### Loss of metallic area:

The same than in the main body of the rope

Class of rope	Maximum permissible loss of metallic cross sectional area	Reference length
	40 %	500 × d
Stranded ropes	10 %	$30 \times d$
	6 %	6 × d

#### Additional:

- ➤ Value on tucks is > 1,10 (1.08) times nominal-Ø (for detachable grips)
- ➤ Rope-Ø is reduced more than 10 % of the nominal-Ø
- ➤ Waviness between the tucks is higher than 0,06 times the nominal-Ø
- Visible fretting between the strands at shrunken tuck tail ends

#### Attention:

Known broken wires on tuck tails do not count!

Repairing actions are recommended, if any discard criteria is reached!

Side 19

# **Knowable damages on Splices**

## tucks

- Deformed tucks, inappropriate support
- Lose wires, fretting, wire breaks

#### Shrunken tuck tail ends

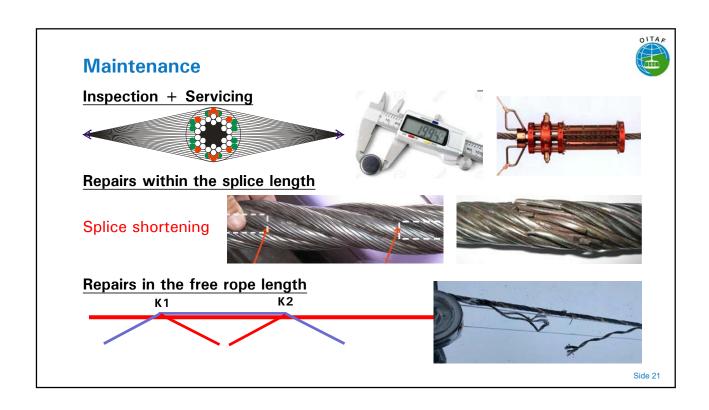
- > Shrunken tuck tail ends
  - = Risk of malfunction of grips
- > Fretting, wire breaks

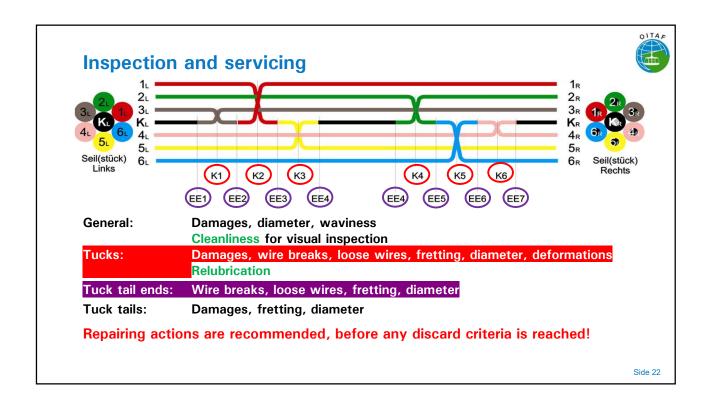
#### Area above the tuck tails

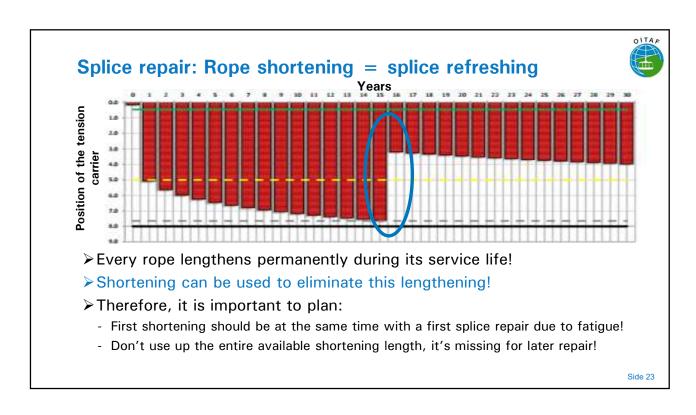
- Uneven strand distribution, malfunction of the wrapping material
- Reduced Diameter = Fretting
  / Risk of malfunction of grips

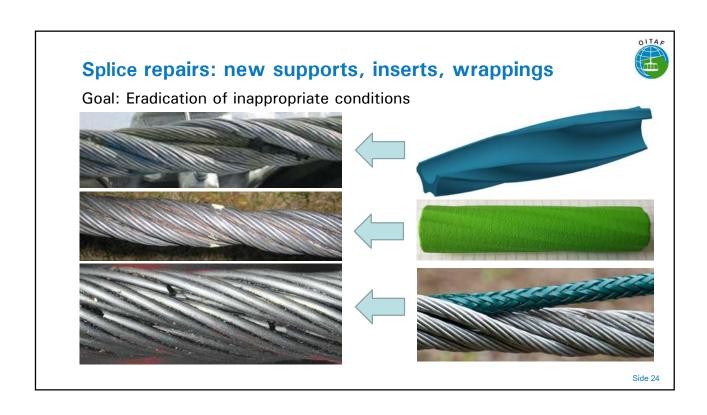












# Splice repair: new inserted additional strands



Goal: Repair of a bigger damage with strands within the splice length

Variant 1: One or two strands are inserted and ends within the splice length



Variant 2: One or two strands are inserted and ends outside of the splice



Attention: Keep remaining strands from the initial splicing, they could be useful for such a repair!

Side 25

# Splice repair: Inserted repair peace



Goal: Repair of a big damages within or near of the splice

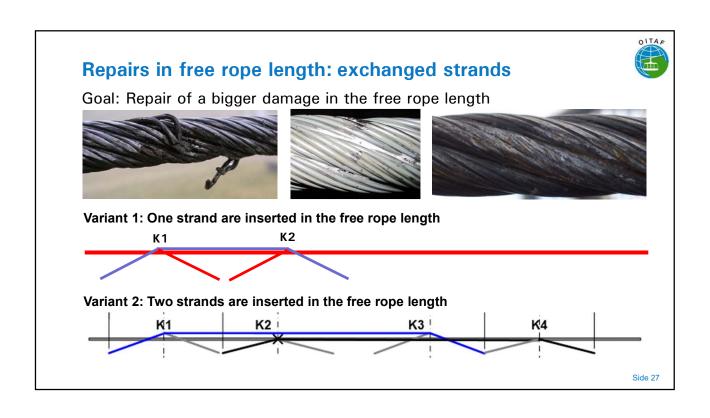


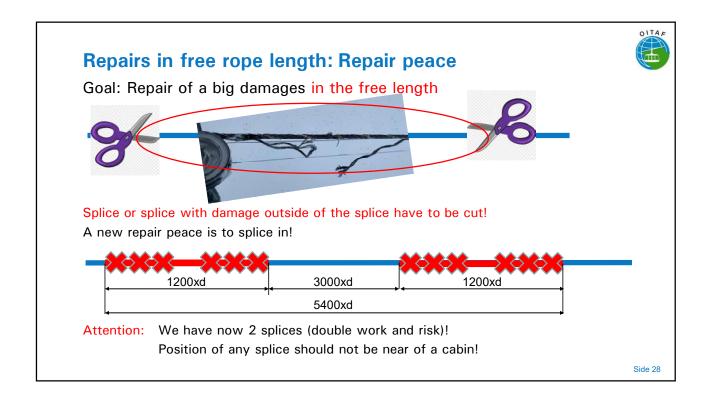
Splice or splice with damage outside of the splice have to be cut out! A new repair peace is to splice in!



Attention: We have now 2 splices (double work and risk)!

Position of any splice should not be near of an end fixing or clamp!





# OITAF

# **Splice lifetime**

# Important for a long splice lifetime are:

- ➤ No damages from incidents
- > suitable, diameter-stable wrapping material
- suitable, diameter-stable material for tuck support
- ➤ Diameter of tucks as big as possible / Place for the additional strand!
- Good support lubrication and relubrication of the tucks
- > suitable, diameter-stable material for inserts between the tuck tail ends
- Good, experienced hand work



Enables bending cycles in the range of 200' – 400'000 BW until repair becomes necessary!

Regular inspection and relubrication of the tucks are indispensable!

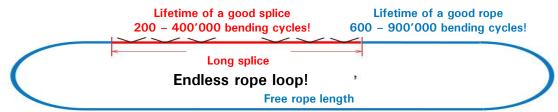
Side 29

# Rope lifetime (free Example)

# OITAR

# Important for a long rope lifetime are:

- ➤ The lifetime of a splice, without shortening, have to be at least ~0.4 as a normal rope lifetime!
- ➤ Short a rope never too much, a part of the length is necessary for later shortenings / splice refreshing's or repairs!
- > Mostly, it is only possible to make two appropriate rope shortenings.



➤ If you take care of the splice, you can use the whole rope for long time and save money!

# **History / Future**

# 1931: Publication H. Overlach, TU Karlsruhe

- Force curve over tuck tails
- Minimum length of tuck tailsMinimum length of the long splice

100 x d

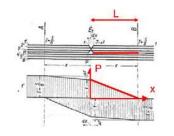
1200 x d

1970 - 2020

- Optimizing of wrapping material, the tuck supports and inserts
- Reduction of the tuck tail length (USA 30xd / CH 50xd)
- 2004 New EN standard required tuck tail length of 60xd

#### 2022

- Up to 50% length reduction of a long splice acc. to EN 12927 (proven, evaluated for each individual splice, with EN certificate)





Side 31



Vielen Dank für ihre Aufmerksamkeit!





Grazie per la vostra attenzione!