

Introduction of Work Committee (WC) II «Ropes»

Chairman:Sven WinterVice Chair / Protocol:Stéphane Pernot

#Manufacturers: Doppelmayr, Leitner Ropeways, Fatzer, Jakob Rope Systems, Teufelberger-Redaelli, Usha Martin

#Testing Bodies: IFT University of Stuttgart, IWM, Letscan, ROTEC, TÜV SÜD, TVFA

#Authorities: BAV, BMVIT, IKSS, INTI, STRMTG

#Operators: Bayerische Zugspitzbahn, Sommerbergbahn Bad Wildbad, Sandia Peak Tramway, Zermatt Bergbahnen

Interested guests or new members with rope experience are welcome!



Introduction of Study Commission (SC) II «Ropes»

Meetings usually 2 times per year

2018 Argentina | Berlin 2019 Winterthur | Garmisch-Partenkirchen 2020/21 online 2022 online | Stuttgart 2023 Oberstdorf



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OITAF Introduction of Working Group «Ropes» Paper 28 / 2014 General recommendations for the manufacturers OITAF lubrication and the re-lubrication of steel wire ropes use in ropeway installations for Passengers BOOK 30 O. I. T. A. F. Paper 3-1 / 2015 BOOK-3-1 Survey of magnetic rope testing of steel wire ropes Possibilities to impr visual rope inspectio Paper 30 / 2019 Possibilities to improve visual rope inspection (VI) Close to finishing and publishing: Ropelifetime Aublished in Sentember 2015

New Paper: Rope Lifetime

* Focus on Stranded Ropes *

Basics about wire ropes used in ropeways

- Wire manufacturing, strand and rope designs
- Transport & assembly
- Rope end connections

Operational influences, e.g.:

- Vehicle clamps
- Rollers, sheaves
- drive, speed

Unscheduled influences, e.g.:

- twist, damage events, environment, heat, ...
- Special incidents out of experience of the group members



New Paper: Rope Lifetime

Degradation mechanisms

Free rope length – fatigue, wear/abrasion, corrosion Splice and end connections – wear/abrasion, twist

Theoretical lifetime estimation by calculation

Lifetime estimation by Feyrer / University of Stuttgart Special Interest: lifetime estimation method of Leipzig

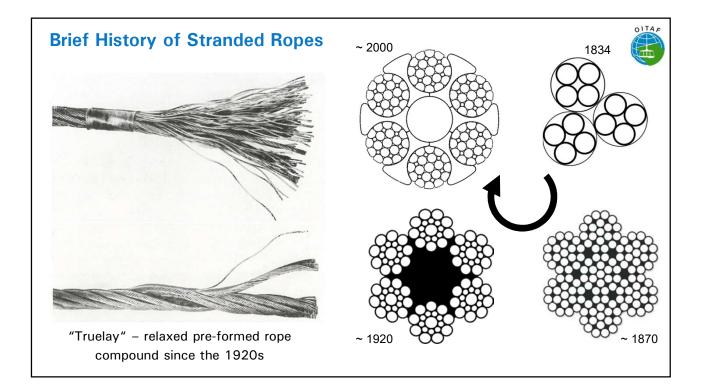
Example Calculations

Discussion of Results



Historical Introduction

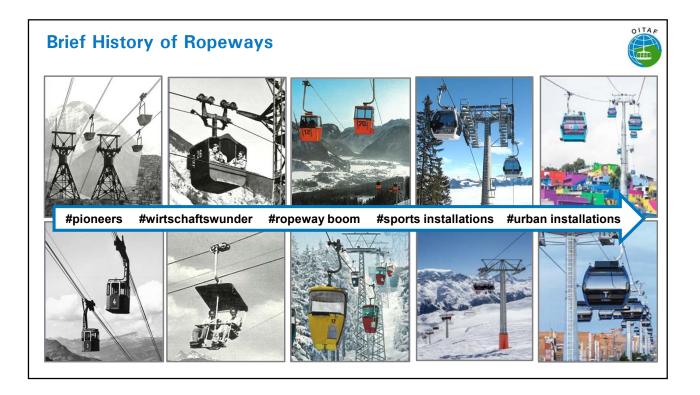
		Y
1834	Invention of the wire rope	7-(
1890-1920	Material ropeways by Bleichert & Co.	1
end 1920s	First passenger ropeways	
since ~1927	Research / 1st bending-tests in Karlsruhe and Stuttgart	
1936	Patent magneto-inductive rope testing	
		ID AR
1980s	First versions of Feyrer Formula	C XT
2000 + +	Online monitoring, lifetime calculations	
2005	European Standardization	
		10
Future	Inspection Intervals based on bending cycles	
		3/11

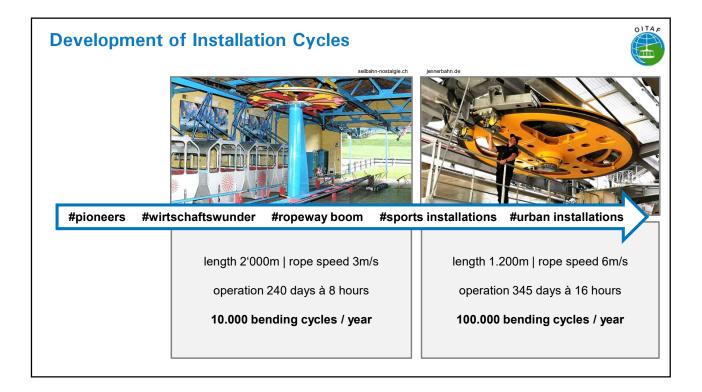


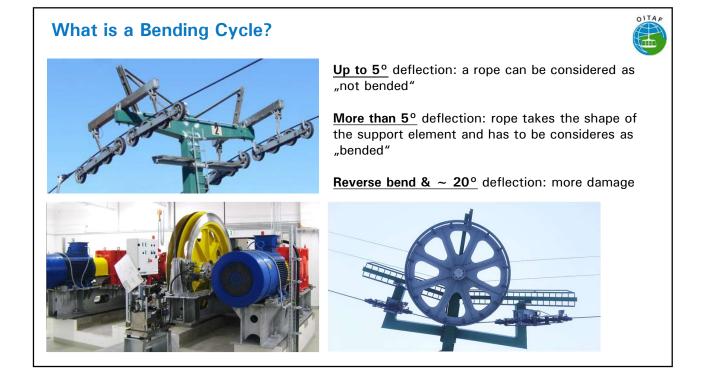
3,5 m

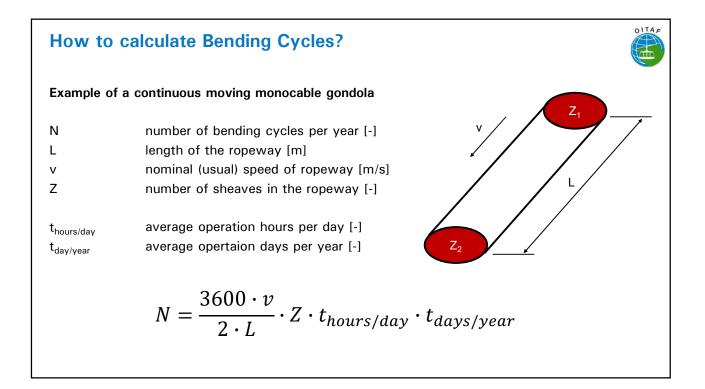
Alberts Dauerprüfe

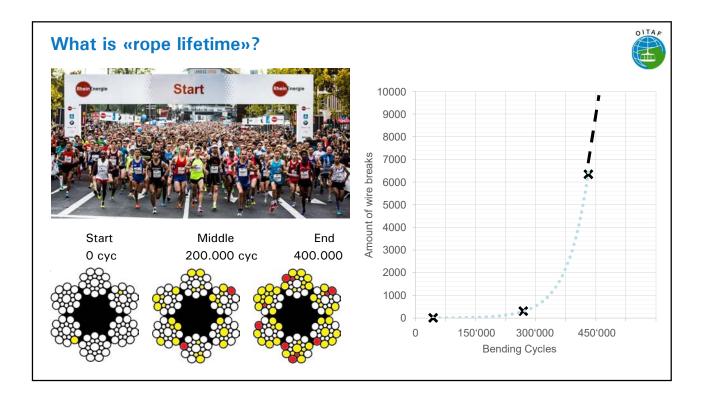
1550 kg











What is «rope lifetime»?

Ropes will develop fatigue, wear and possibly local damage within (long-term) operation

Target: operate ropes as long as possible in safe conditions

Limit: "discard maturity" – defined conditions under which a wire rope must be replaced

Examples for point of discard

- · Local damage (which cannot be repaired any more)
- · Safe inspection is no more possible
- Increase of wire breaks will be too fast for feasible future inspection intervals
- · development of wire breaks is not safely predictable

We do not want to witness rope failures – we want to keep safe conditions and change a rope on time.



«Overall package» of OITAF SC II Ropes

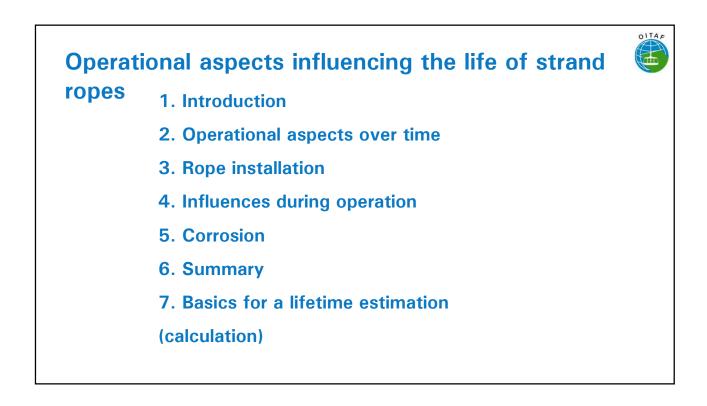


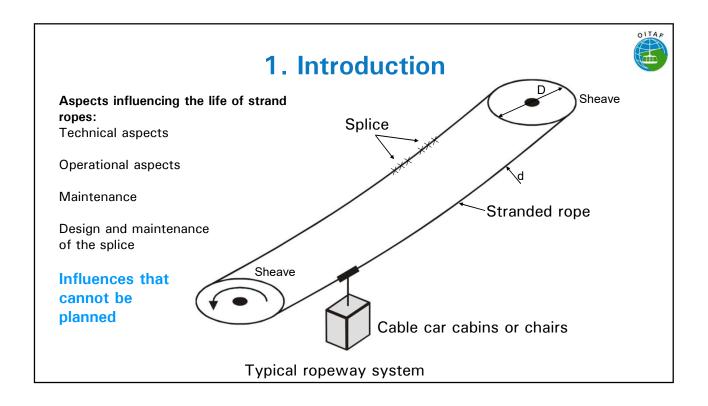
Visual Inspection Magnetic testing Lubrication Rope lifetime management

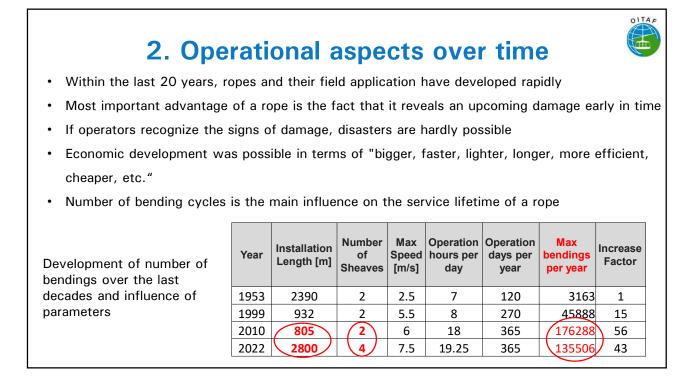
- -> sustainable use of a rope
- -> planable maintenance actions
- -> preventive maintenance
- -> safe ropeway operation
- -> cost efficiency











3. Rope installation

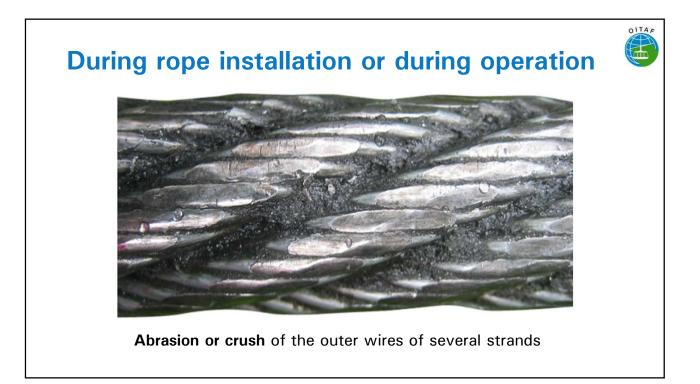


 $\ensuremath{\textbf{Abrasion}}$ - critical situation, rope too close to the soil



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Contact with obstacles - disastrous situation



Rope installation and maintenance



Improvised clamp missing groove unsmooth surface unknown sliding force OITAF



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4. Influences during operation

Differences in rope tension forces lead to changes in the lay length, in torque and twist, but also to different transverse forces. Fatigue and abrasion may occur.

Expected different rope tension results from:

- · Height difference bottom station mountain station (haulage rope)
- Difference of rope tension before drive wheel after drive wheel
- Load condition
- Dynamic forces from acceleration / deceleration
- Meteorological influences (temperature, wind, ice, etc.)

Unexpectedly fast changes may occur from heavy storm with gusts, ice shedding, trees fall on ropes, etc.

It is important to remember not to constantly change the driving speed. A constant driving speed protects the system (oscillations / vibrations) and the rope.

and

The energy in the system dependents quadratically from the driving speed.







Environmental influences, Lightning strikes



Lightning strikes not predictable Not reliably detectable by MRT recognisable by visual inspection

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Environmental influences, Heat on rope



Heat impact on a carrying-hauling rope

Heat of fire

damages the outer wires starting at about 200°C

Failure of the core means that the rope compound loses its support leading to touching strands, wear, corrosion and wire breaks

Lubricants can melt from about 60°C or even lose their properties at about 100°C

Ropes should be kept in motion to prevent local rope sections from heat damages

After exposure to heat on ropes, it is essential that they are assessed by competent persons



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Environmental influences, Heat on structures



Heat from sunlight

towers are prevented from heating up by installing sheet-metal panels covering the shafts

Melting of permafrost

leads to deformations, settlements and thus to dis-alignments of the track, to twisting and different lay length, up to rope derailment

Melting of permafrost under drive stations To protect the permafrost from warming up, foundations are specially insulated against the subsoil to prevent disalignments of the track

Derailment and rollovers



Rollover of a hauling rope

Rollover of hauling rope Rollovers can be caused by vibrations due to emergency braking or wind.

Both track rope and hauling rope should at least be visually inspected after such an incident.

Derailments of funicular ropes can happen quite often.

Especially for concave slope designs, in combination with transverse wind, the rope can fail to lay back into the track rollers.

If derailments mainly happen in the passing loop, the rollers may be insufficiently adjusted or worn. In this case, the rope can be damaged over a very long distance.

In any case of derailment, a competent person should be consulted.

Environmental influences, electrical fields



Moving rope in electromagnetic field generates electrostatic charges of the rope.

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At electrically earthed points of contact with the rope, the wires may locally overheat. Increased wire fracture and reduced

lifetime of the rope are the results.

Conclusion

No ropeways near high-voltage powerlines and transmitter-masts.

As a rule, the ropeway control reacts more sensitively than the rope...

Environmental influences, volcanic ashes



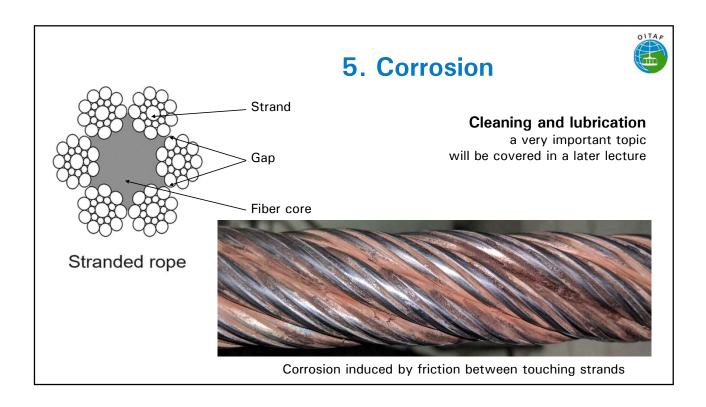
After volcano eruption

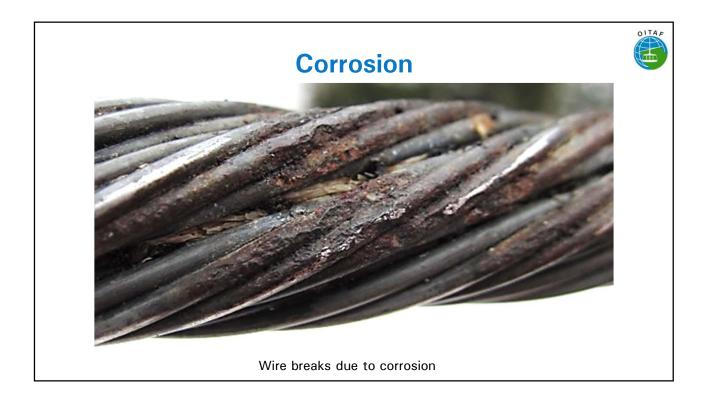
Ropeways in the vicinity of volcanoes are very exposed to atmospheric influences such as carbon, sulfur, salt water, etc.

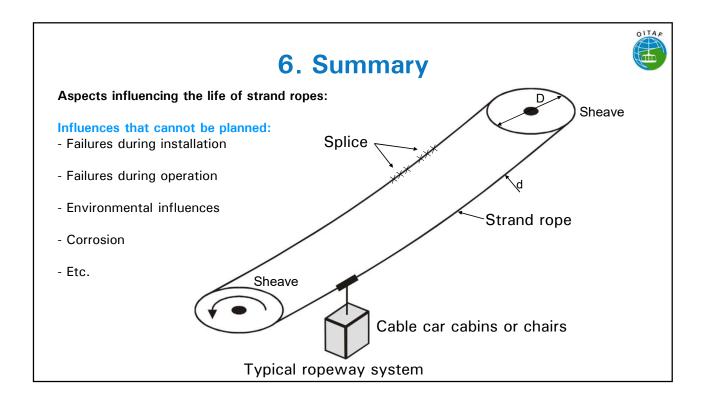
Bright ropes instead of galvanized ropes In this specific environmental condition, the bright ropes shall be advised in respect to the galvanized ropes. In fact, the released sulfur vapors are able to connect with the zinc and create a brittle structure that result in a premature and fast rope failure.

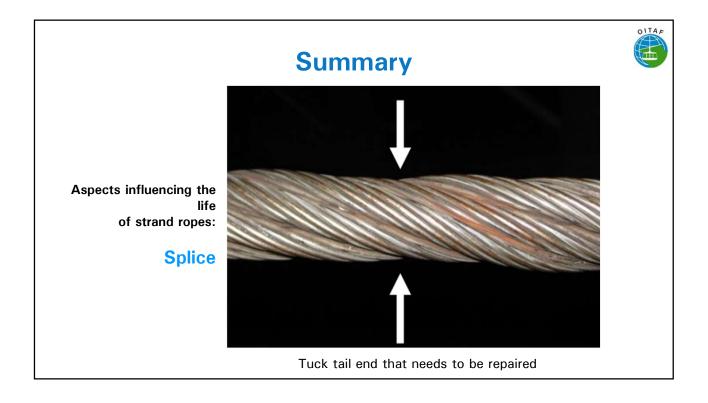
Rope after volcano eruption

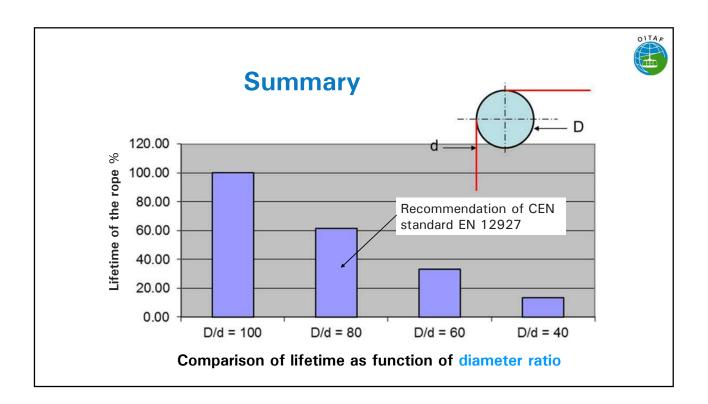
Without cleaning, the lifetime of the rope is greatly reduced

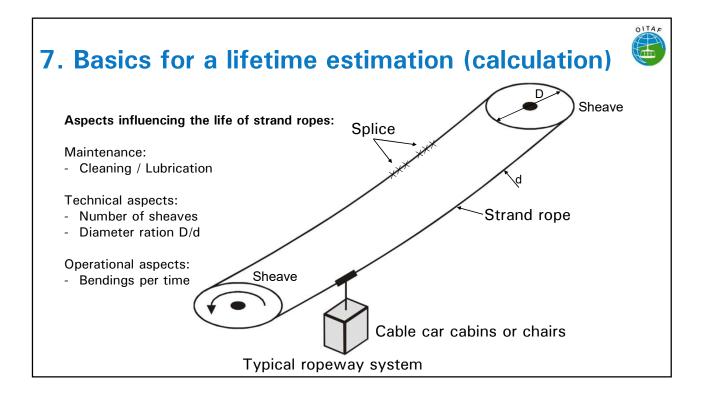


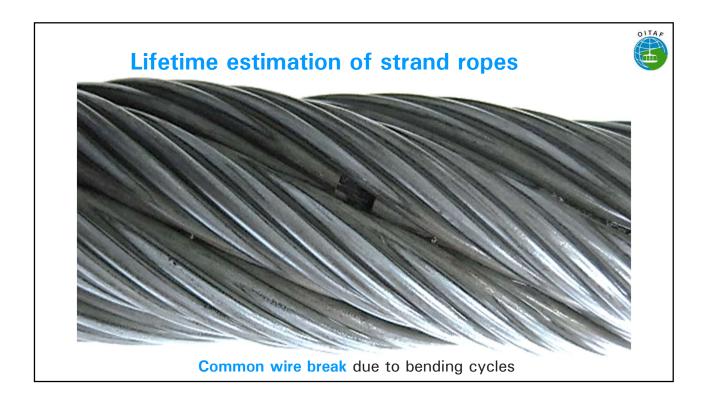






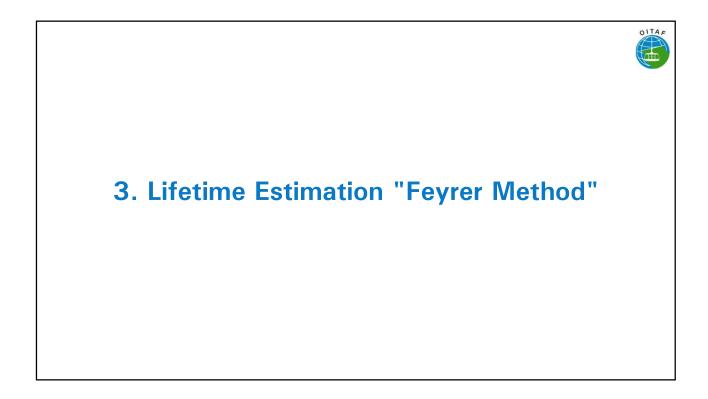


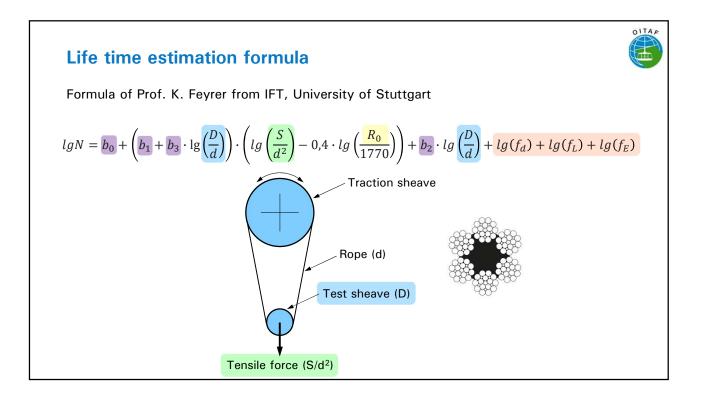




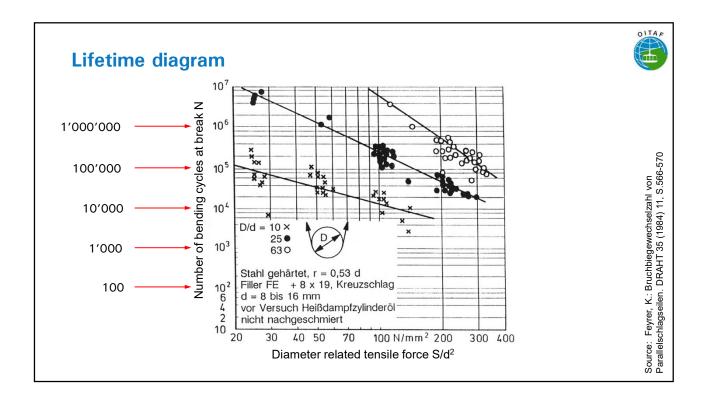


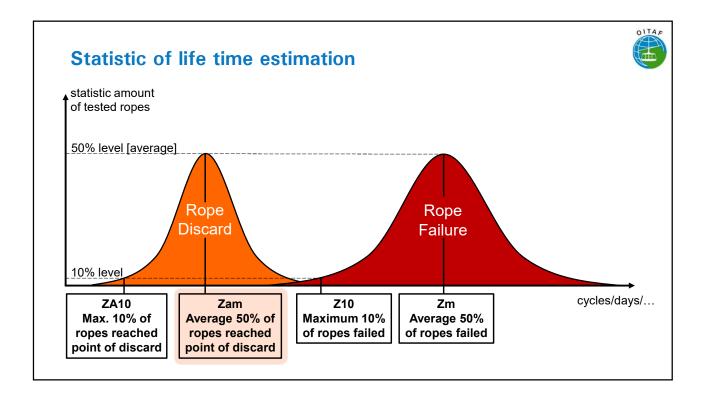












Life time estimation formula

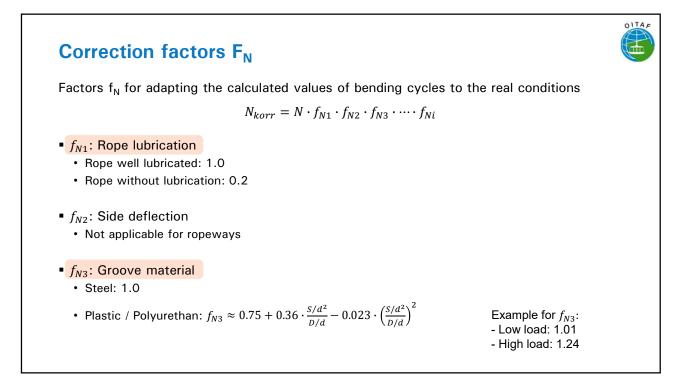
$$lgN = b_0 + \left(b_1 + b_3 \cdot \lg\left(\frac{D}{d}\right)\right) \cdot \left(lg\left(\frac{S}{d^2}\right) - 0.4 \cdot lg\left(\frac{R_0}{1770}\right)\right) + b_2 \cdot lg\left(\frac{D}{d}\right) + lg(f_d) + lg(f_L) + lg(f_E)$$

The formula is valid with following requirements

- Single bending
- · Round steel groove
- Groove radius r = 0.53d
- · No side deflection of the rope
- · Rope generously lubricated with heavy oil or vaseline
- · In dry rooms

Results:

- + $Z_{\rm m}$: Average 50% of ropes broken
- Z₁₀ : Maximum 10% of ropes broken
- + $\rm Z_{am}$: Average 50% of ropes reached point of discard
- Z_{a10} : Maximum 10% of ropes reached point of discard



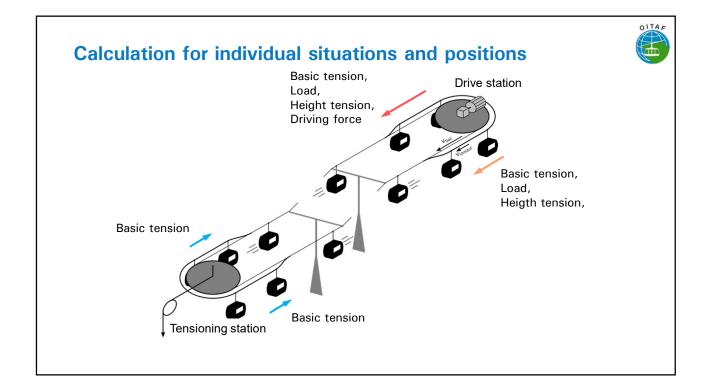
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Factor for rope tensile force

Rope tensile force can vary:

$$S = \frac{Q \cdot g}{n_T} \cdot f_{S1} \cdot f_{S2} \cdot f_{S3} \cdot f_{S4} \cdot f_{S5} \cdots$$

- f_{S1} : Friction in rope drive (roller guide / sliding guide)
- *f*_{S2}: Efficiency of the rope
- *f*_{S3}: Parallel ropes
- *f*_{S4}: Speed / Acceleration
- *f*_{S5}: Bending with changing tensile force



Accumulation of separate lifetime values

 $Z = \frac{1}{\sum_{i=1}^{W_i} N_i}$

Palmgren-Miner Formula:



1. Accumulation: $Z_{Am \ acc.} = \frac{1}{\frac{W_1}{N_1} + \frac{W_2}{N_2}} = \frac{1}{\frac{1}{N_1} + \frac{1}{N_2}}$

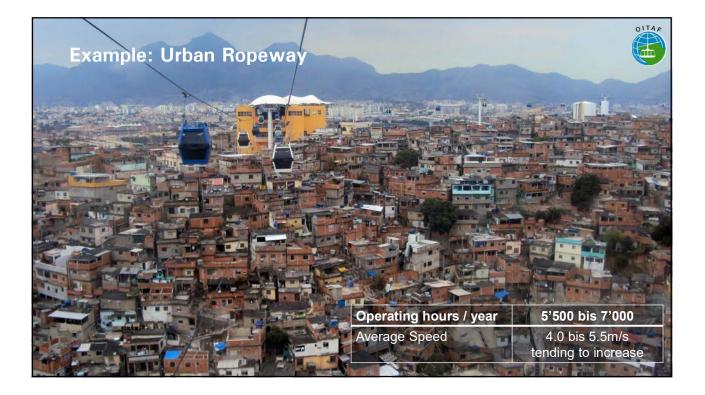
Working cycles accumulated over 2 sheaves for one operation mode

2. Accumulation: $Z_{load} = \frac{1}{\frac{W_1}{N_1} + \frac{W_2}{N_2}} = \frac{1}{\frac{x\%}{N_1} + \frac{y\%}{N_2}}$

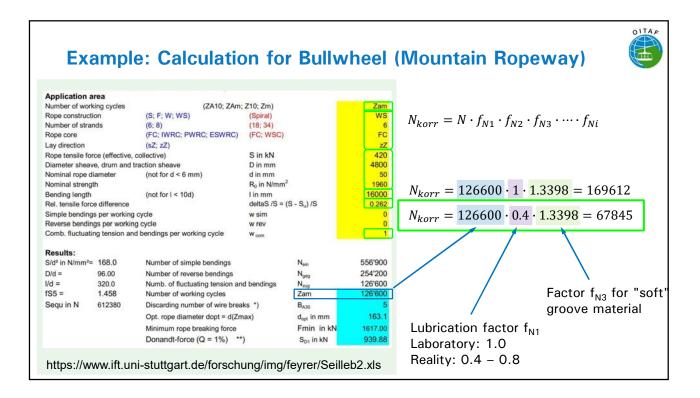
Accumulated working cycles with accumulated portion of operation modes

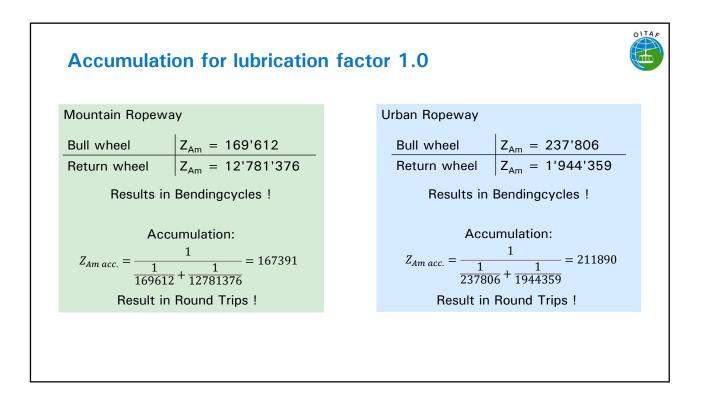


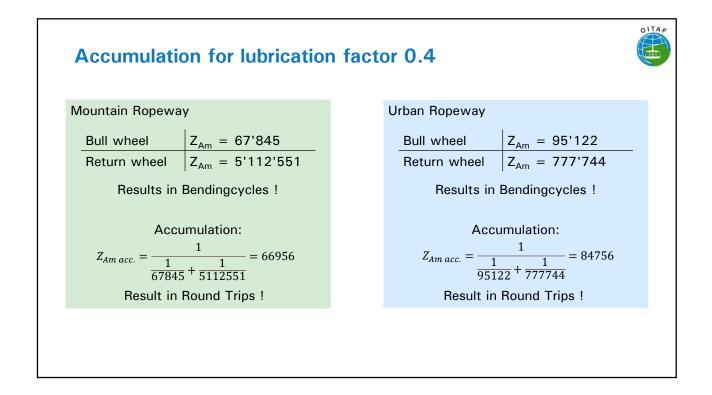


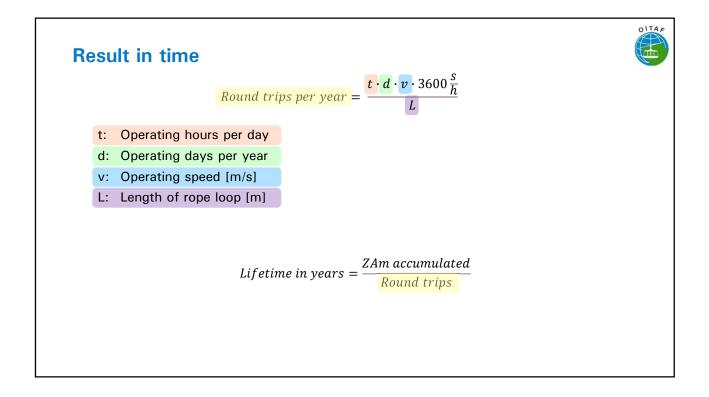


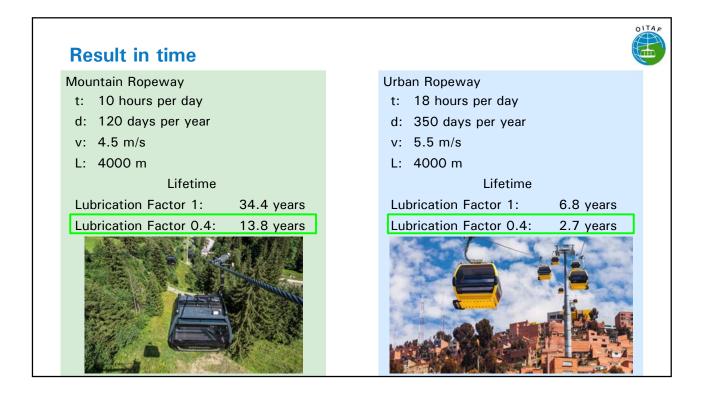
Exam	ole for Calculation		
L	4000 m		4000 m
Н	600 m / 7	ΔH	50 m
	4.5 m/s	v (a)	5.5 m/s
d	50 mm	d	50 mm
D	4800 mm	D	4800 mm
Bull wheel		Bull wheel	
F1 🏄	420 kN	F1	420 kN
=2	310 kN	F2	330 kN
∆S/S	0.262	∆S/S	0.214
-N3	1.3398 ALPE Express	FN3	1.3398
Return wheel		Return wheel	
F1 = F2	190 kN	F1 = F2	320 kN
∆S/S	0	∆S/S	0
F _{N3}	1.0168	F _{N3}	1.1993

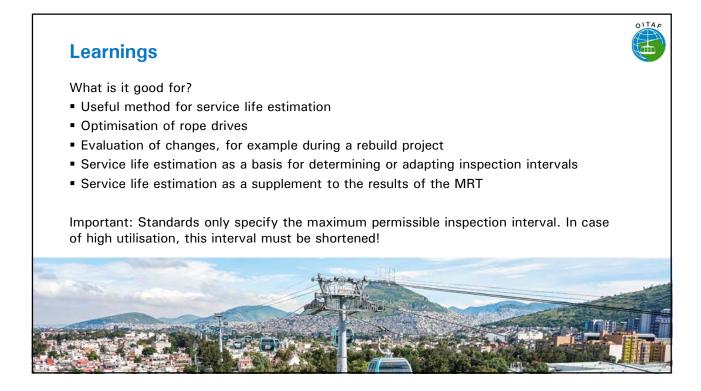






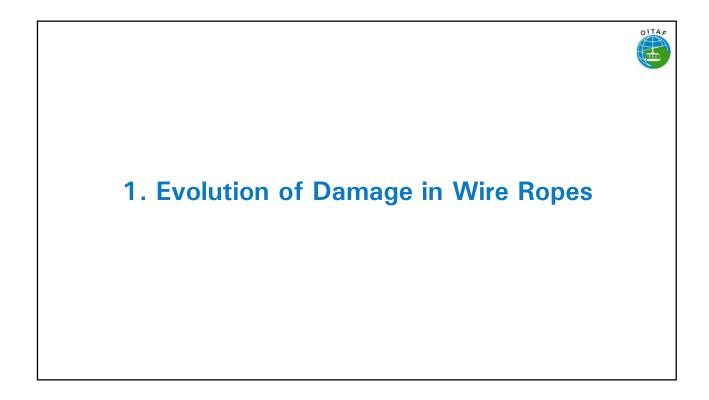


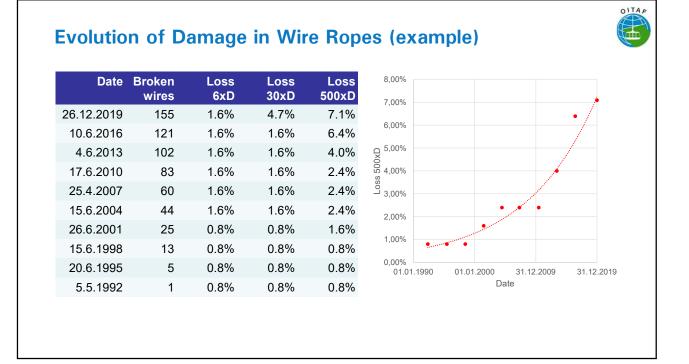


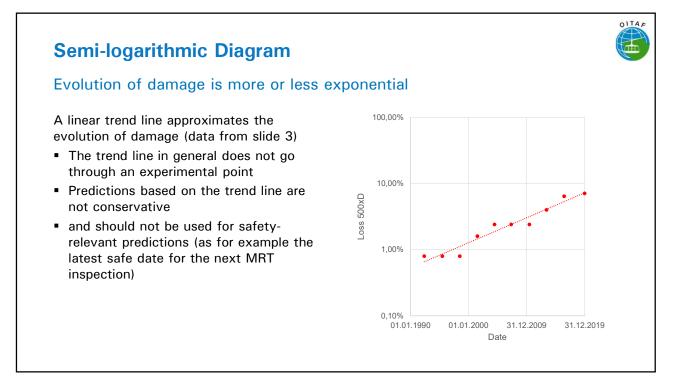










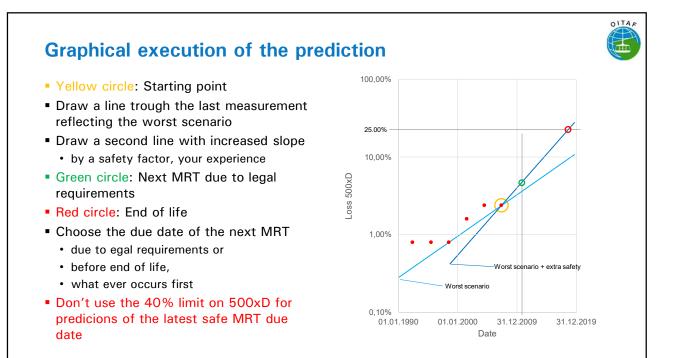


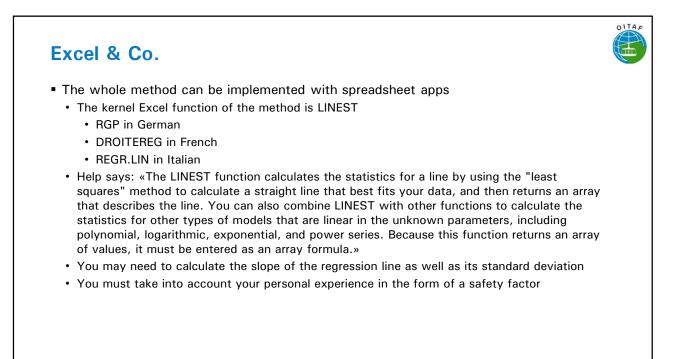
2. Principles of Safe Prediction

Principles of Safe Prediction

- The prediction should start at the current point
- The prediction should reflect the worst scenario imaginable
 (whatever that means)
- Damage mechanisms may change over time
 - A prediction should take this into account in an appropriate way.
- The loss of cross-section is difficult to predict, it may be necessary to couple it to the evaluation of the number of broken wires
 - The loss of cross-section tends to be proportional to the number of broken wires
 - In the case of few wire breaks, this assumption is on the conservative side

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3. Practical application

Application to example (data from slide 3)

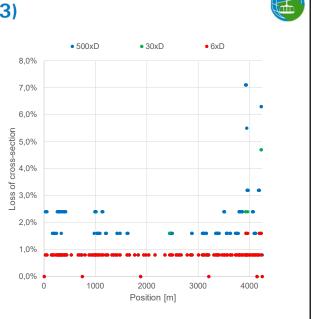
Date	Broken	Prediction	Loss 6xD	Prediction	Loss Pi	rediction	Loss P	rediction
	wires	broken wires		6xD	30xD	30xD	500xD	500xD
26.12.2019	155	191	1.6%	2.5%	4.7%	2.5%	7.1%	10.3%
10.6.2016	121	162	1.6%	2.5%	1.6%	2.5%	6.4%	6.4%
4.6.2013	102	144	1.6%	2.8%	1.6%	2.8%	4.0%	4.2%
17.6.2010	83	123	1.6%	3.3%	1.6%	3.3%	2.4%	4.9%
25.4.2007	60	99	1.6%	3.6%	1.6%	3.6%	2.4%	5.4%
15.6.2004	44	72	1.6%	2.3%	1.6%	2.3%	2.4%	4.6%
26.6.2001	25	54	0.8%	3.3%	0.8%	3.3%	1.6%	3.3%
15.6.1998	13		0.8%		0.8%		0.8%	
20.6.1995	5		0.8%		0.8%		0.8%	
5.5.1992	1		0.8%		0.8%		0.8%	

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- The broken wires in the most-damaged region were visible
- The operator repaired the rope in this region after the rope inspection of the 26.12.2019
- The results of later MRT's are not shown here, because they are no longer comparable
- The distribution of the rope damage on the 26.12.2019 is shown in the diagram



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Conclusions

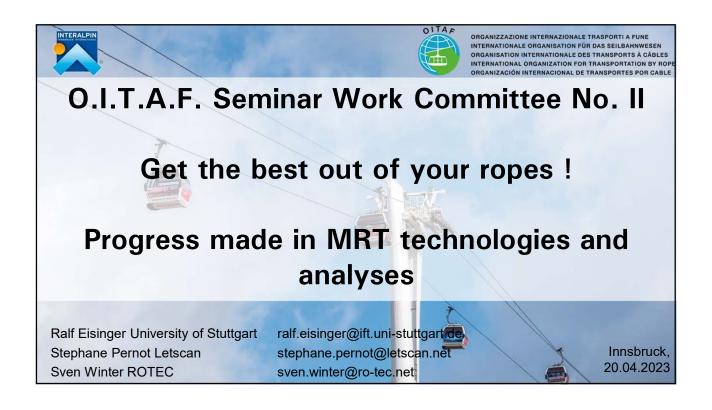


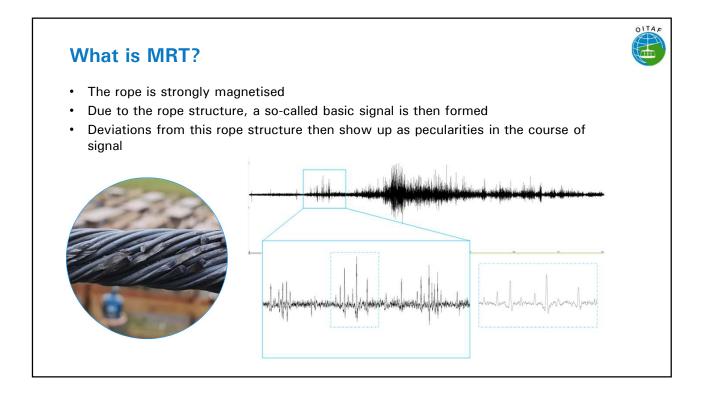
- Pro's:
 - · We have 20 years of experience with predictions based on MRT results
 - · The method safely predicts the evolution of damage over one MRT period
 - We have only a few MRT results exceeding the prediction (< 1 / year with 500 MRT / year)
 - · The method is very powerful in estimating safe MRT periods
 - · The method handles the distribution of damage correctly

Con's:

- Implementation in Excel is complex and error-prone
- The quality of the prediction decreases with reference length
- The predictions for the reference length 6xD are not very reliable







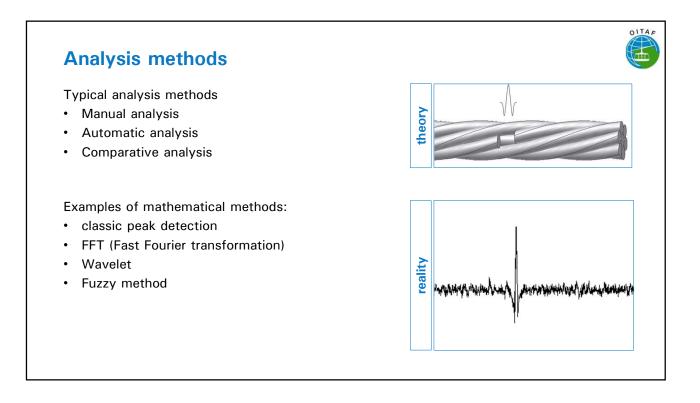
Technical aspects

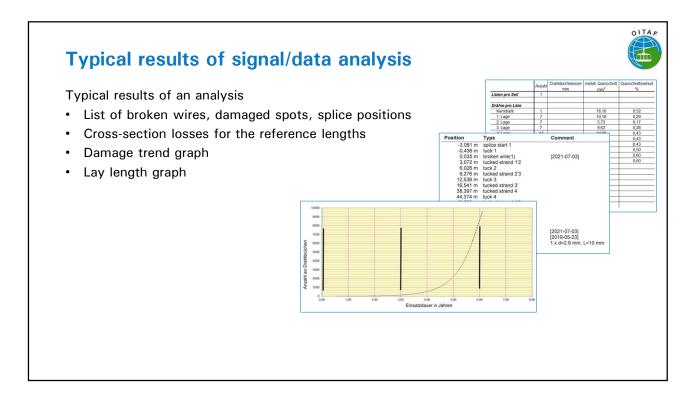
Magnetic field generation

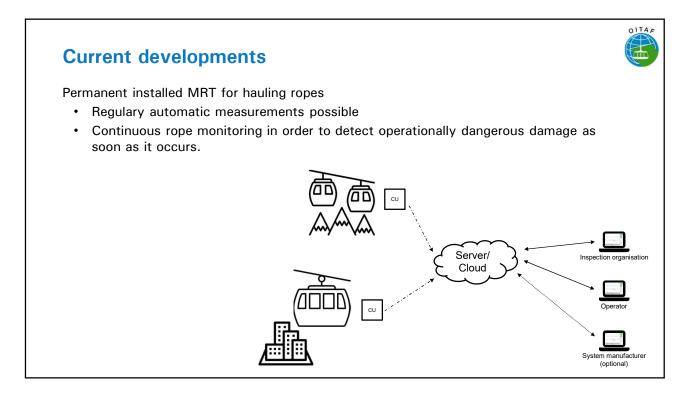
- Permanent magnet
- Electromagnet

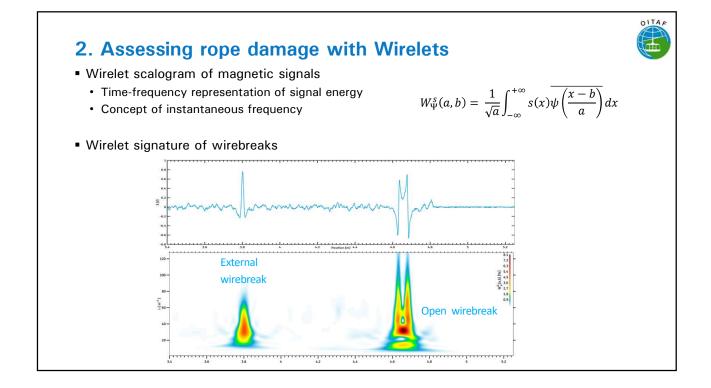
Sensors

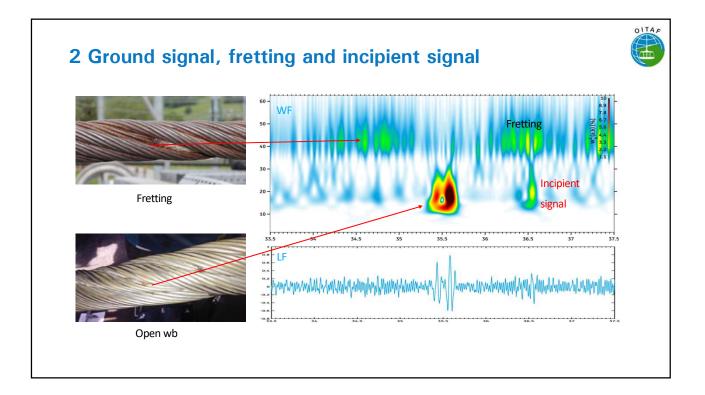
- (Classical) coil
 - Change of magnetic field
- Speed dependent
- Hall effect sensors
 - Absolute value of the magnetic field

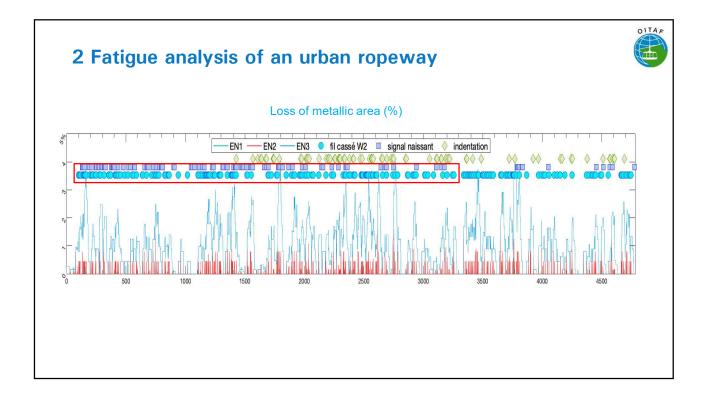


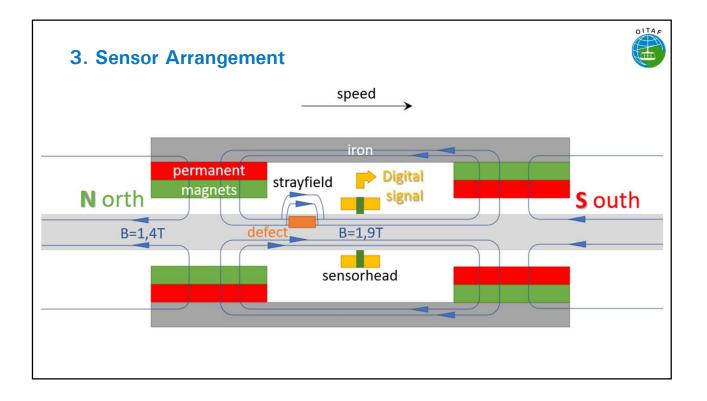


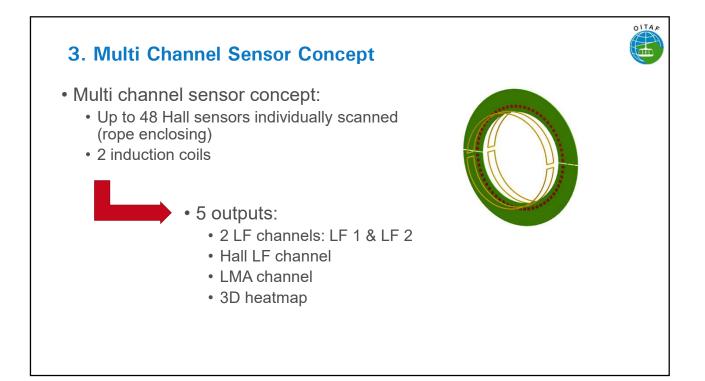




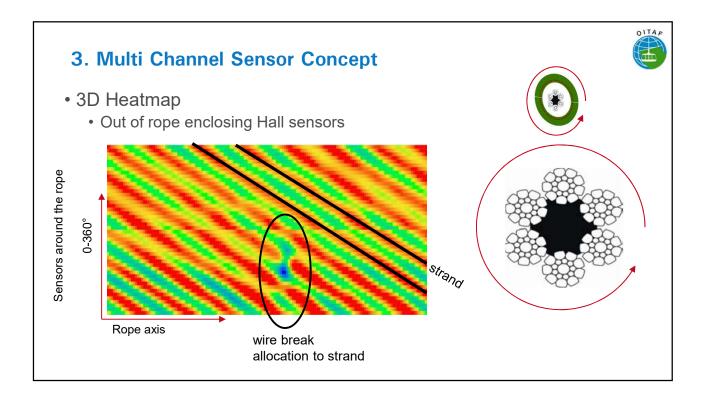


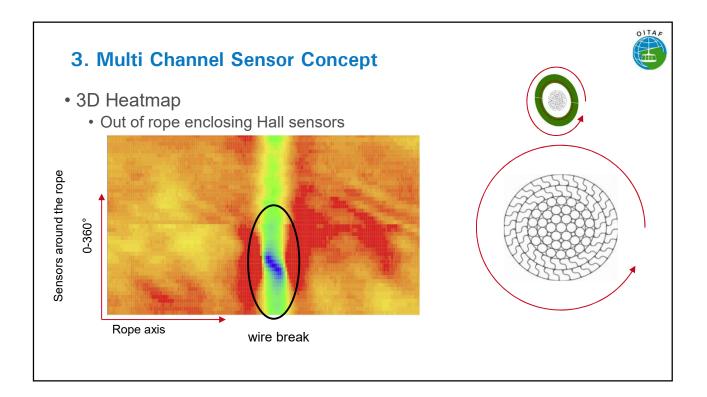


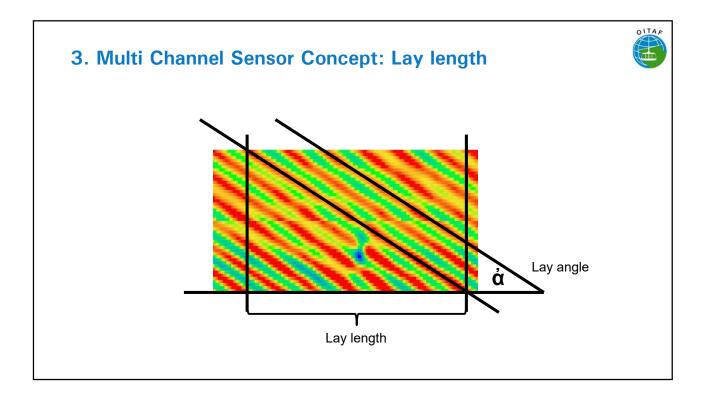


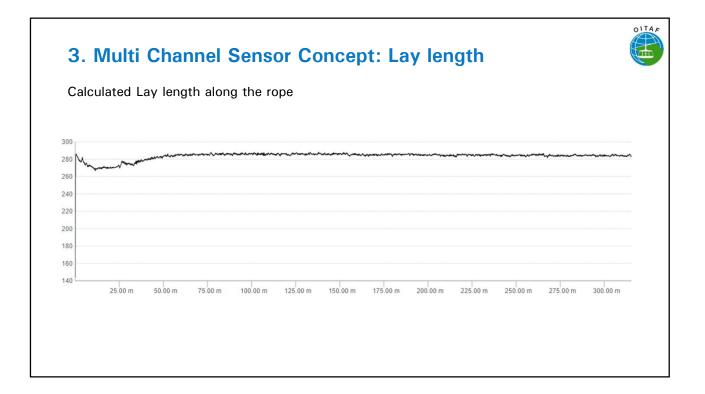


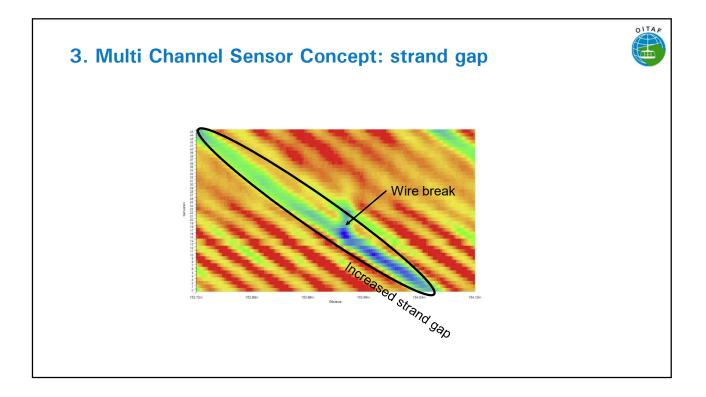
Channel	LF 1 & LF 2	Hall LF	LMA	3D Heatmap	
type	Induction coils	Hall sensors	Hall sensors	Hall sensors	
		0	0	0	
category	Local Fault	Local Fault	Loss of Metallic Area	Local Fault	
Type of defect	Broken wires (Wear, corrosion)	Broken wires (Wear, corrosion)	Wear, Corrosion	Broken wires geometry faults (lay length)	
Advantage	Redundancy: Independent Channels		absolute value	3D representation Location info	
Min. Speed	0,3 m/s	0 m/s	0 m/s	0 m/s	





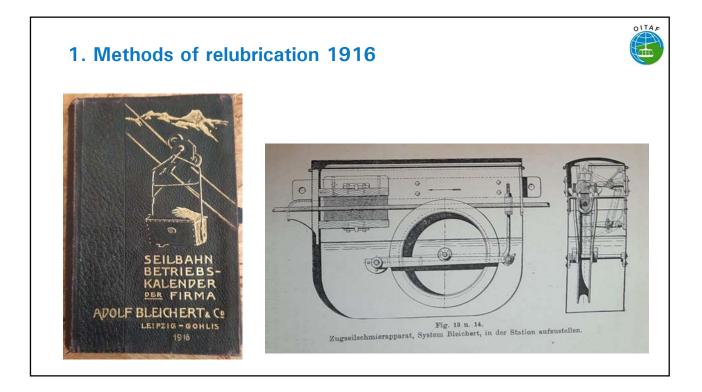








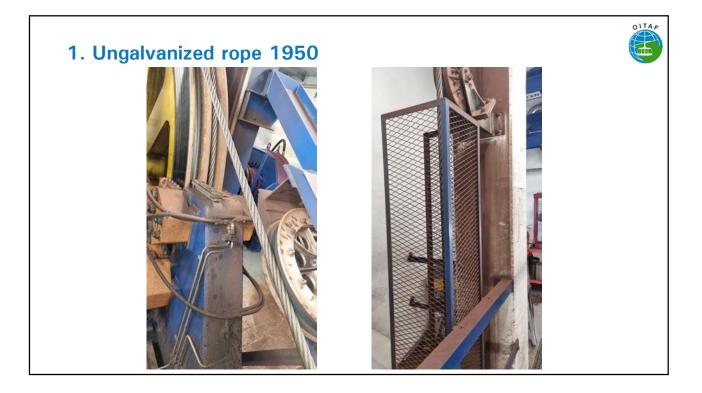












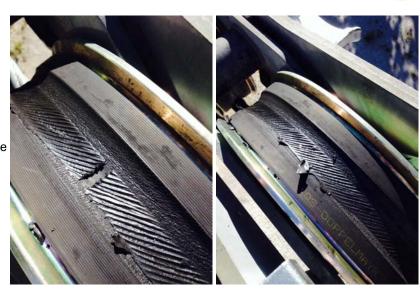
1. Galvanized rope 1960

Since the 1960s, galvanized ropes became more and more common.

Corrosion was no longer a problem

Due to the contamination of the ropeway and passengers, the primary lubricant and relubrication were increasingly reduced or neglected.

Rope lubrication got a negative image



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1. Galvanized rope 1960

Due to unsuitable relubricant, the roller rubbers were dissolved and damaged.

As a result, a large number of the track rollers had to be replaced prematurely.

For this reason, the operators have significantly reduced or completely stopped relubrication.



2. Lack of basic lubrication in today's haulage ropes

Very low basic lubrication for a new rope



At rope opening after 4 years of operation



After two years of operation, there is already significant corrosion on the strands

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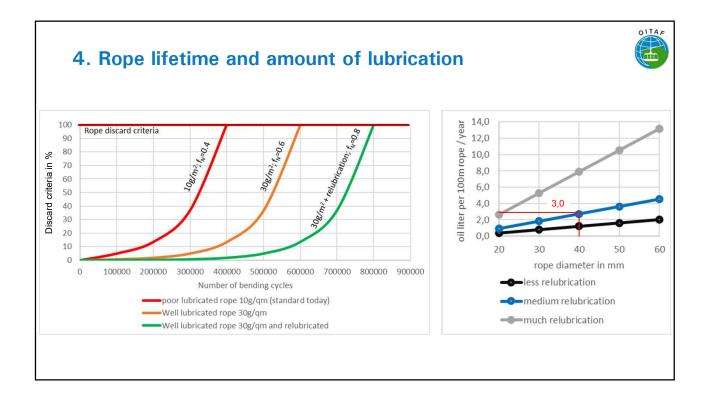
3. Primary lubrication and relubrication requirements

Primary lubrication:

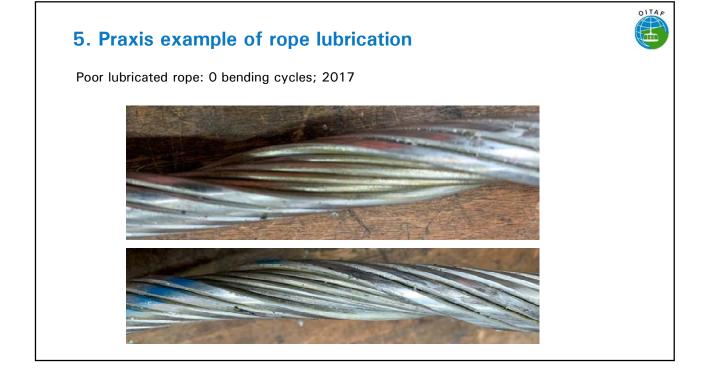
- Uniform distribution of the lubricant during stranding
- For good basic lubrication, approx. 30 g/sq. m. of wire surface should be applied.
- For a 40 mm rope (rope weight 6kg/m), it is approx. 75 g per meter of rope

Relubrication:

- Relubrication should be frequent or permanent during operation
- The relubricant must be compatible with the base lubricant
- The relubricant should be creepable so that it reaches the inside of the strand.
- The relubricant must be compatible with the roller rubbers



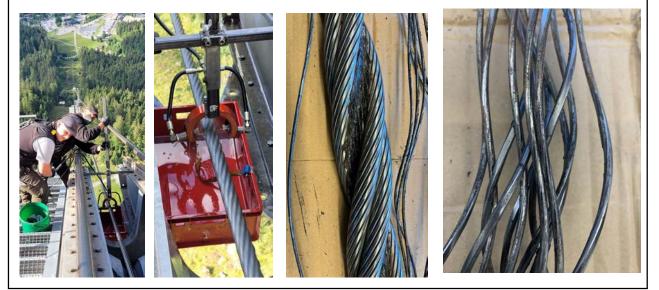
OITAA





6. Methods of relubrication

Interval relubrication: Result of the same rope after well relubrication



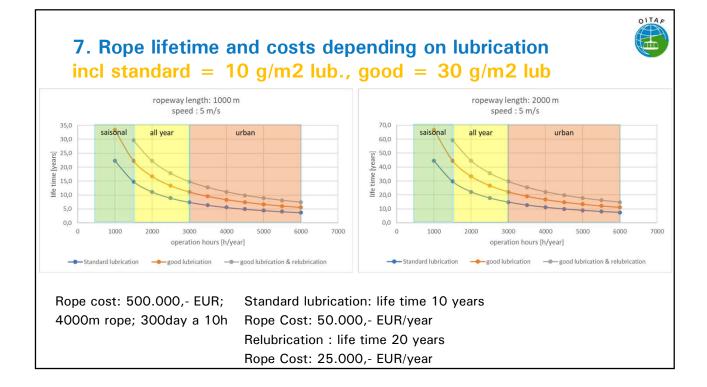
6. Methods of relubrication

Permanent oiling dependent on rope speed



OITAF

OITAF

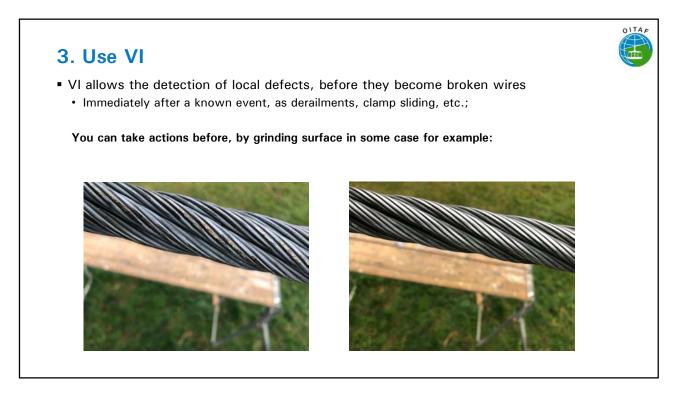






OITAF 1. Rope installation & splice Choice of rope · Finish of wire as needed (environmental conditions) Installation of a rope · Organize a correct transport, storage and installation of a rope Replacement of the rope · Check interfaces, for example groove New rope diameter Old rope diameter diameter Old rope New rop • Splice : see presentation of Focus on Splices Bruno LONGATTI (IKSS, CH) ure at edd groove used by old cable



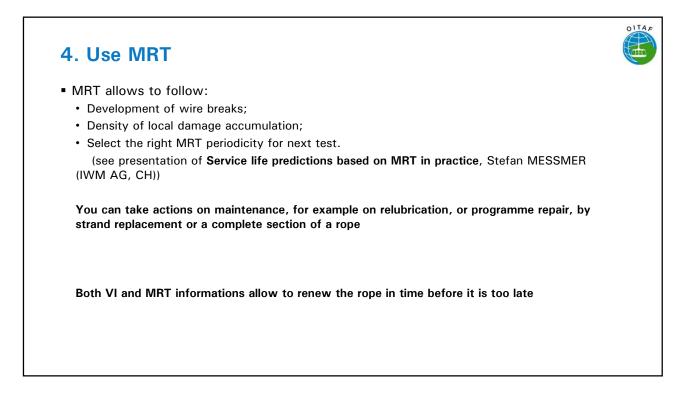


3. Use VI

- OITAF
- VI allows the detection of local defects, before they become broken wires
 - At the normal periodicity for undetected event, as lightning strikes, scratches and notches, for examples.

You can take actions before, by grinding surface in some case for example:

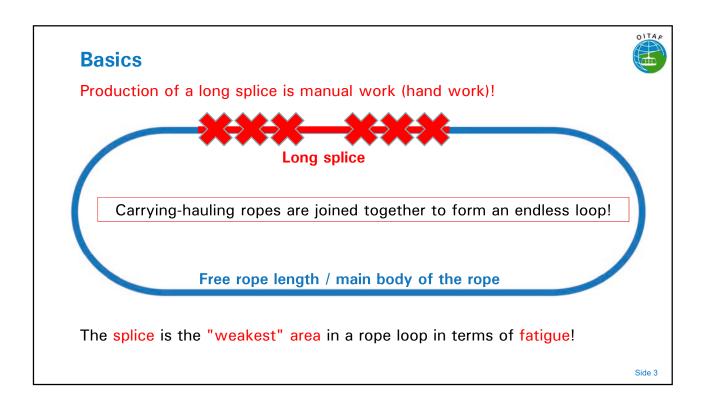




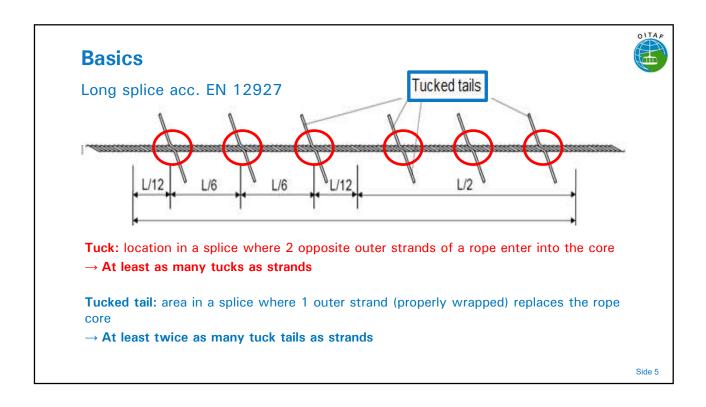


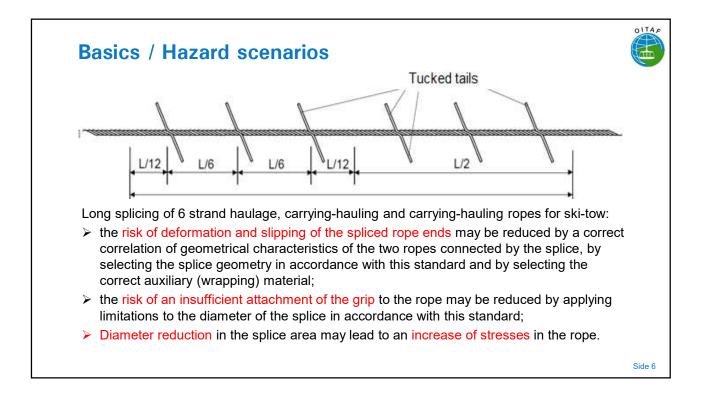


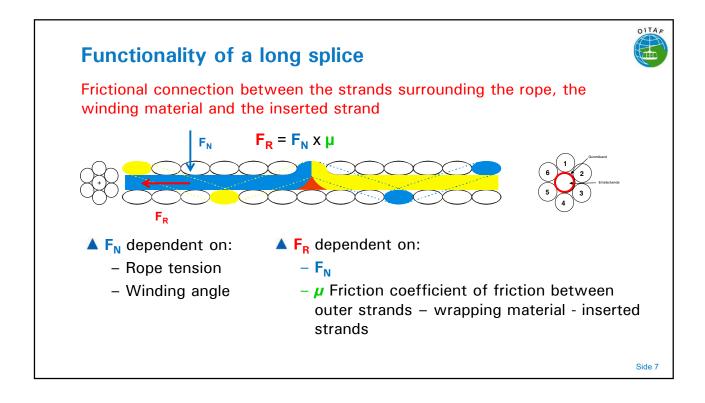




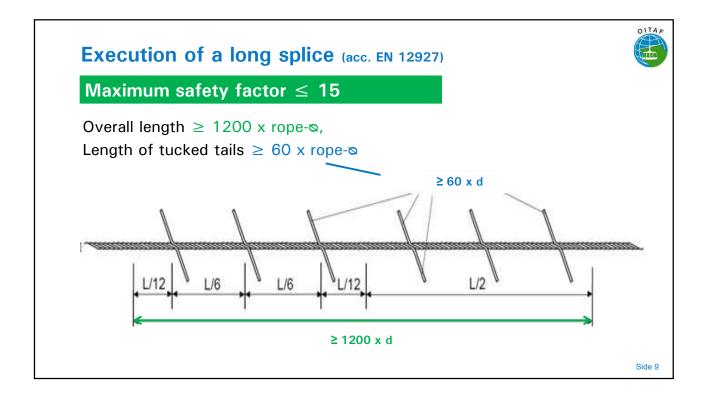


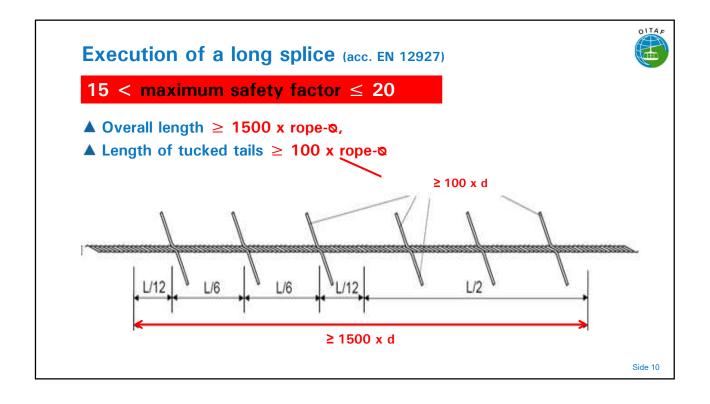


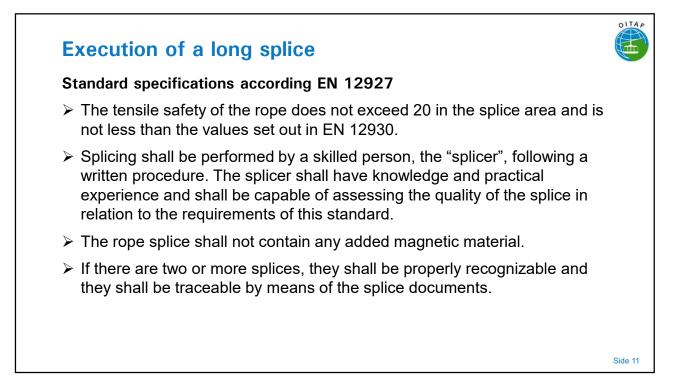


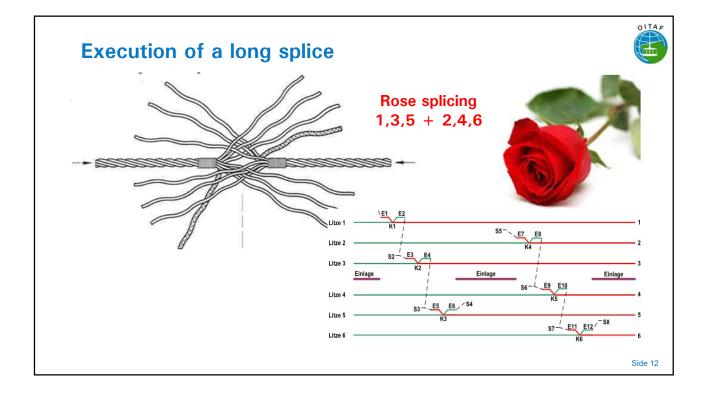


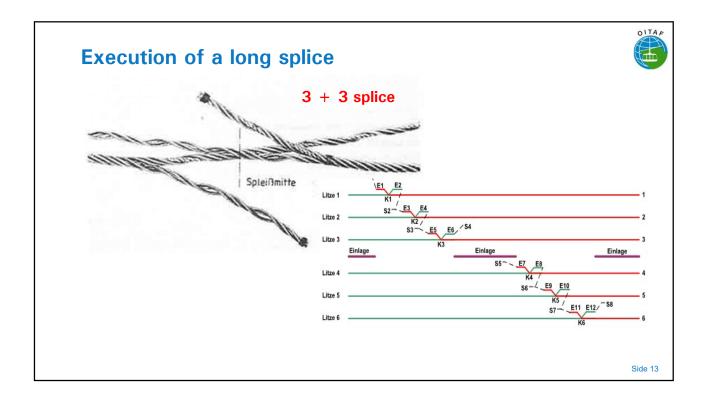
Variables:	Recommendations:		
Total length of a long splice	> = 1200 or 1500		
Length of tuck tails	> = 60 or 100		
Diameter of tucks whole splice area	< = +8% (10%) of nominal Ø > = -10% of nominal Ø		
Waviness within the splice area	< 6% of nominal Ø		
Splice version	no requirements		
Wrapping material of the tuck tails	no requirements		
Splice tucks execution type	no requirements		
Type of splice tuck supports	no requirements		
Type and design of the inserts	no requirements		

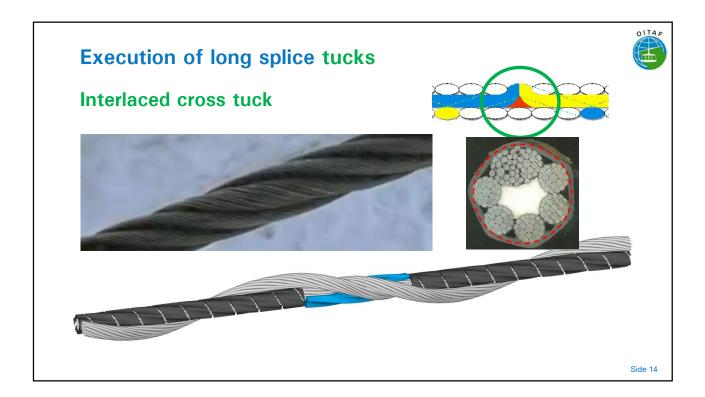


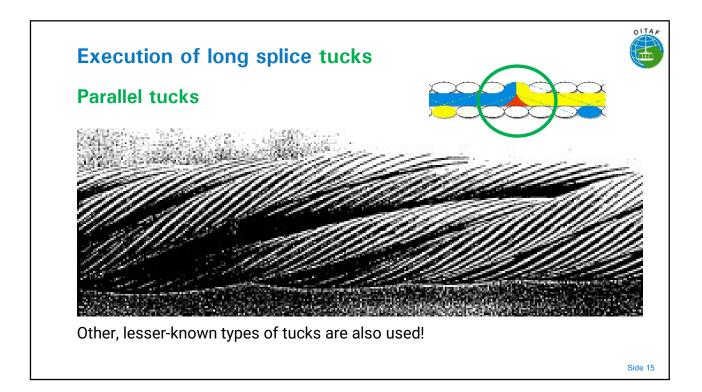


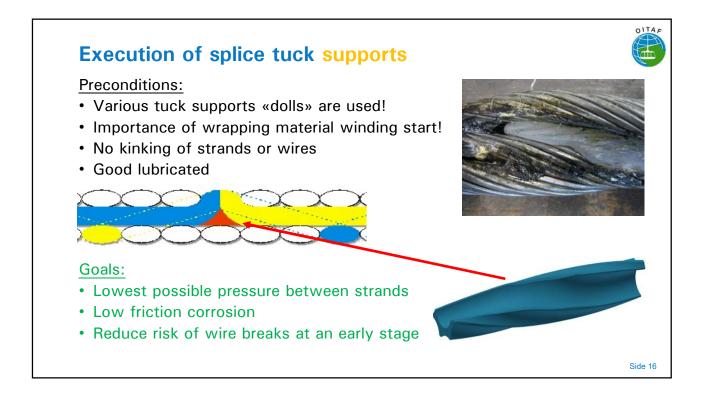












Execution of the tuck tail wrapping

Preconditions:

- Various wrapping materials are used for doubling up the inserted tuck tails and creating friction
- Wrapping material is durable, flexible

Goals:

- Preventing metallic contact between the inserted tuck tails and the outer strands
- Reduce risk of fretting and wire breaks at an early stage



OITA

OITA

Execution core portion between tuck tail ends

Preconditions:

- Various inserts are used!
- Diameter of the inserts is big enough
- Insert is durable
- Tuck tail ends are close to each other or to the insert

Goals:

- Reduce risk of shrunken tuck tail ends
- Reduce risk of fretting and wire breaks at an early stage

Attention: Damages at tuck tail ends are difficult to repair!

